# 12148 Albion Vaughan Road Bolton, ON Traffic Impact \& Parking Study 

Paradigm Transportation Solutions Limited

## Project Summary

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# 12148 Albion Vaughan Road Traffic Impact \& Parking Study 

## Executive Summary

## Content

This report is an update to the November 2020 study previously prepared. This update reflects changes to the site plan and development statistics, as well addresses review comments from the review agencies following the first development application submission.

This study has been prepared in support of a proposed residential development for a site located at the municipal address of 12148 Albion Vaughan Road in the community of Bolton, Town of Caledon, Region of Peel.

The development as proposed consists of two residential towers, one six-storey tower and one seven-storey tower. In total the overall development proposes a total of 265 residential dwelling units. A total of 462 parking spaces would be provided on-site to serve the development. Vehicular access would be provided via full-movement driveway connections with Albion Vaughan Road. A total of 156 bicycle parking spaces will also serve the development ( 84 long-term and 72 short-term spaces).

The study assesses the weekday AM and PM peak hour traffic impact of the proposed development, provides a review of the parking requirements, and a functional review of the proposed site plan.

## Conclusions

The conclusions of the study are as follows:

- Under the base year conditions, all study area intersections operate at acceptable levels of service and within capacity.
- For the 2029 background traffic conditions (without subject development), all study area intersections are forecast to operate at acceptable levels of service and within capacity.
The exception would be the Regional Road 50 and Albion Vaughan Road/Mayfield Road intersection, where the overall intersection v/c ratio is forecast to be 0.95 during the AM peak hour. The southbound dual through movement is reported to operate with a v/c of 0.94 during the AM peak hour.
- Under the 2029 total traffic conditions (with subject development), all study area intersections are forecast to operate at acceptable levels of service and within capacity.

The previously identified critical movements would continue to be reported, albeit slightly exacerbated.

- The overall impact of the proposed residential development is anticipated to be minimal. The development is estimated to generate and add a total of 105 and 104 vehicle trips to the adjacent transportation network during the AM and PM peak hours, respectively.

The additional traffic would be less than daily traffic variations typically experienced. It is determined the site generated traffic would increase volumes at the study area intersections between 1.0 to 2.3\%.

While not identified as a critical movement, auxiliary dual leftturn lanes were investigated at the westbound approach at the intersection of Regional Road 50 and Albion Vaughan Road/Mayfield Road intersection. The movement is acknowledged to be approaching capacity under 2029 background and total traffic conditions.

As analyzed with dual left-turn lanes on the westbound approach and optimization of signal timing splits within exiting cycle lengths, the overall intersection is reported to operate at acceptable levels of service and with all movements within capacity under the 2029 horizon.

- At the main central site access intersection with Albion Vaughan Road, it was determined an auxiliary northbound left-turn lane would be warranted from a volume perspective. It is noted that the auxiliary left-turn lane is not required from an operational standpoint.
- The proposed overall parking results in a theoretical deficient of 2 spaces in comparison to the minimum zoning by-law requirements. That is, the visitor parking requirements would be satisfied; however, the proposed resident parking requirements would be theoretically deficient by $0.5 \%$.

The proposed resident parking supply is anticipated to adequately serve the residential development. The main basis in support of the minor reduction is supported by ITE Parking Generation forecasts of peak parking demands. The proposed resident supply would result in a surplus of parking based upon the forecast peak demands. Additionally, parking spaces will be unbundled from residential units.

- A review of the site plan was undertaken. No major conflicts or issues were identified for the anticipated design vehicles expected on-site.


## Recommendations

The recommendations of the study are as follows:

- From a transportation perspective, the planning applications sought should be approved as the development is determined to have a minimal impact on the adjacent transportation network.
- The intersection volumes and operations at the Regional Road 50 and Albion Vaughan Road/Mayfield Road intersection be monitored by the applicable jurisdiction to determine when dual westbound left-turn lanes should be provided.
- Regardless of being warranted, a northbound auxiliary left-turn lane is not required at the central site access intersection on Albion Vaughan Road based upon forecast traffic operations.


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## 1 Introduction

### 1.1 Overview

This report is an update to the November 2020 study previously prepared. This update reflects changes to the site plan and development statistics, as well addresses review comments from the review agencies following the first development application submission.

Paradigm Transportation Solutions Limited (Paradigm) was retained to conduct this Traffic Impact and Parking Study for a proposed residential development in the community of Bolton (Town of Caledon).
Figure 1.1 illustrates the location of the subject site situated on the west side of Albion Vaughan Road, north of Regional Road 50.

### 1.2 Purpose and Scope

The purpose of this report is to identify and assess the potential traffic impacts of the proposed development. The scope of the study was developed in consultation with Town of Caledon staff via e-mail correspondence in October 2020.

The study has been updated based on review comments received from Town of Caledon staff dated 06 August 2021. At the time of writing of the original study, Region of Peel staff had not responded to our request for pre-study consultation. It is further noted that following the initial development application submission, Region of Peel staff did not have any review comments on the transportation study deliverable.
Appendix A contains the original terms of reference and pre-study consultation completed with Town staff.

The scope of this study is as follows:

- A study area comprising the following intersections:
- Peel Regional Road 50 and Albion Vaughan Road/Mayfield Road;
- Albion Vaughan Road and Kirby Road; and
- Albion Vaughan Road and the proposed central site access driveway.
- Traffic forecasts for 2029, representing a five-year horizon following anticipated build-out/occupancy in 2024;
- Weekday AM and PM peak hour analysis time periods;
- A review of parking to confirm the proposed supply will be adequate for the proposed use; and
- A review of the design of site accesses, internal circulation, and loading areas to confirm they will accommodate the vehicles expected on-site.

The methodology used in this study is summarized below:

- Estimate the future peak hour background traffic for the horizon year by applying a $2 \%$ per annum growth rate as advised by Town staff;
- Estimate the net increase in vehicular traffic with the proposed development;
- Combine the future background traffic with the net increase in site traffic to determine the total traffic volumes under the horizon year;
- Analyze existing, future background, and total traffic conditions;
- Determine the net impact on operational performance due to site traffic, and the need for road and/or traffic control improvements to address the identified impacts; and
- Use of AutoTURN software to prepare on-site vehicle maneuvering diagrams.

This study has been carried out in general accordance with the Region's TIS Guidelines ${ }^{1}$, pre-study consultation comments and addressed review comments received from Town staff. Appendix A contains the pre-study correspondence and comments.

[^0]

## Study Area and Site Location

## 2 Proposed Development

The subject site is located at the municipal address of 12148 Albion Vaughan Road. The subject lands are currently occupied by a detached single-family home which would be demolished to facilitate redevelopment of the lands.

Figure 2.1 illustrates the site plan. The proposed residential development consists of two residential towers. In total the overall development proposes a total of 265 residential dwelling units. The development statistics are as follows:

- One six-storey residential tower with 114 units total:
- 37 one-bedroom units;
- 22 one-bedroom + den units;
- 31 two-bedroom units;
- 18 two-bedroom + large balcony units;
- 6 three-bedroom units.
- One seven-storey residential tower with 151 units total:
- 41 one-bedroom units;
- 14 one-bedroom + den units;
- 68 two-bedroom units;
- 21 two-bedroom + large balcony units;
- 7 three-bedroom units.

The entire development would be served by several at-grade parking spaces and a two-level underground parking structure. A total parking supply of 462 spaces serving residents and visitors are proposed onsite.

A total of 156 bicycle parking spaces ( 72 short-term and 84 long-term) are proposed on-site. Out of the 72 short-term spaces, 30 spaces are proposed at-grade and 42 spaces are proposed in the two-level underground parking structure. All 84 long-term bicycle parking spaces are located within secured storage rooms in the underground structure serving residents.

Three full-movement access driveways are proposed, with two of the three driveways providing dedicated access to the loading area serving each residential tower (i.e., service vehicles only). The main central vehicular access serving the development provides access for building residents and visitors.

For assessment purposes it is anticipated full build-out and occupancy will occur by 2024.


## 3 Existing Conditions

### 3.1 Roads and Traffic Control

The characteristics of the roads and intersections in the vicinity of the subject site are described below. Reference is made to the Town of Caledon's Official Plan - Schedule J: Long Range Road Network². The main roadways that form the study area comprise Albion Vaughan Road-Mayfield Road, Regional Road 50, and Kirby Road. Each roadway is described as follows:

- Albion Vaughan Road is a north-south, two-lane, undivided roadway that operates under the jurisdiction of the Town of Caledon. The road is classified as a medium capacity arterial per the Town's Official Plan, additionally this roadway is identified as the Proposed Bolton Arterial Route (BAR). The roadway has a rural cross section, with gravel shoulders on both sides. The posted maximum speed limit is $60 \mathrm{~km} / \mathrm{h}$ within the study area limits;
- Mayfield Road (Peel Regional Road 14) is an east-west, twolane, undivided roadway that operates under the jurisdiction of the Regional Municipality of Peel. The road is classified as a major road under the Region's Official Plan and a high capacity arterial per the Town's Official Plan. The roadway has a semiurban cross section. The posted maximum speed limit is 60 $\mathrm{km} / \mathrm{h}$ within the study area limits;
- Highway 50 (Peel Regional Road 50) is a north-south fourlane undivided roadway that operates under the jurisdiction of the Regional Municipality of Peel. The road is classified as a major road under the Region's Official Plan ${ }^{3}$ and a high capacity arterial per the Town's Official Plan. The roadway has an urban cross section north of Albion Vaughan Road/Mayfield Road, and a semi-urban cross section south of Albion Vaughan Road/Mayfield Road. The posted maximum speed limit is 80 $\mathrm{km} / \mathrm{h}$ within the study area limits;
- The intersection of Regional Road 50/Albion Vaughan RoadMayfield Road is currently signalized with auxiliary left and right turn lanes are provided on each intersection approach; and

[^1]- The intersection of Albion Vaughan Road/Kirby Road forms an unsignalized " $T$ " intersection. Stop control is provided on the westbound Kirby Road approach.

Figure 3.1 illustrates the existing lane configurations and traffic control devices at the study area intersections.


## Existing Lane Configurations and Traffic Control

### 3.2 Transit Services

The study area is currently served by limited transit routes/services.
Within the community of Bolton, the Town of Caledon has retained Voyago to provide local service (began November 11, 2019). The local transit line in Bolton includes 39 new bus stops along the route with service running during peak commute hours (Monday to Friday between 6:00 AM and 9:30 AM, and from 3:00 PM and 6:30 PM). Within the study area, local transit service operates along Regional Road 50.

GO Transit provides bus service to the Regional Road 50/Mayfield Road Park and Ride located on the southwest corner of the intersection of Regional Road 50 and Albion Vaughan Road/Mayfield Road. The following route is operated by GO Transit:

- Route 38 (Bolton) operates between Downtown Bolton and Malton GO Station. Service is provided Monday to Friday only. The northbound route operates from 4:45 PM to 7:15 PM. The southbound route operates from 5:16 AM to 6:01 AM.


### 3.3 Active Transportation

Sidewalk and separated bicycle infrastructure is not provided on Regional Road 50 or along Albion Vaughan Road. Pedestrians and cyclists are expected to utilize the gravel shoulder on either roadway or share the travelled roadways with vehicles.

A review of the Region of Peel's Active Transportation Implementation Plan ${ }^{4}$ did not identify any existing cycling or pedestrian facilities on the study area roadways. The Long-Term Regional Pedestrian Network (Caledon) proposes sidewalks on the west and east sides of Regional Road 50 ; however, no horizon year for their implementation is currently known.

The Proposed Long-Term Regional Cycling Network (Caledon) proposes bike lanes on Regional Road 50; however, no horizon year for their implementation is currently known as well. Further review of the Town of Caledon's "Explore Caledon" cycling map identified that no cycling facilities are provided on Albion Vaughan Road.

The walk phases incorporated into the signal timing plan for the Regional Road 50 and Albion Vaughan Road/Mayfield Road intersection are push button actuated for pedestrians to cross Regional Road 50 . The pedestrian phase is always provided for both the

[^2]northbound and southbound through phases. Pedestrian signal heads are provided for each approach crossing. The existing volume of crossing pedestrians at this intersection during the weekday AM and PM peak hours was found to have zero pedestrian crossings.

### 3.4 Modal Split

To gain a better understanding of existing travel characteristics of the subject site and surrounding area, 2016 Transportation Tomorrow Survey (TTS) data was reviewed for TTS Zone 3190. Zone 3190 is bounded by Queensgate Boulevard, Regional Road 50, and Albion Vaughan Road.

The existing mode share for travel during the weekday AM and PM peak periods has been reviewed. Inbound and outbound trips during the morning three-hour travel period (6:00 AM - 9:00 AM) and the afternoon three-hour travel period (4:00 PM - 7:00 PM) were assessed. Table 3.1 summarizes the existing modal splits.

TABLE 3.1: EXISTING MODAL SPLIT

| Mode | AM <br> Inbound | AM <br> Outbound | PM <br> Inbound | PM <br> Outbound |
| :--- | :---: | :---: | :---: | :---: |
| Auto Driver | $84 \%$ | $76 \%$ | $88 \%$ | $85 \%$ |
| Auto Passenger | $6 \%$ | $13 \%$ | $9 \%$ | $14 \%$ |
| Transit | $0 \%$ | $2 \%$ | $2 \%$ | $0 \%$ |
| Cycle | $0 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| Walk | $10 \%$ | $9 \%$ | $1 \%$ | $1 \%$ |
| Total | $\mathbf{1 0 0 \%}$ | $\mathbf{1 0 0 \%}$ | $\mathbf{1 0 0 \%}$ | $\mathbf{1 0 0 \%}$ |

Inbound and outbound trips during the AM peak period are predominately automobile based accounting for $90 \%$ of trips, whereas $10 \%$ of the trips are made via walking. This relatively high percentage of walking trips appears to be attributed to school-related trips.

Similarly, PM peak period trips are predominantly automobile based. Automobile trips account for $97 \%$ of PM inbound trips and $99 \%$ of PM outbound trips.

### 3.5 Traffic Volumes

Turning movement counts (TMC) quantify the volume and type of vehicles travelling through an intersection. The TMC data is typically collected during peak travel periods to capture peak traffic volumes and patterns.

Beginning in March 2020 the Province of Ontario implemented restrictions for day-to-day activities in response to the COVID-19 global pandemic. Restrictions included the closure of all school institutions
under further notice, reduced gathering sizes which has results in limited operations at places of employment. At the time of writing, restrictions were in place to varying degree. As a result, typical travel volumes and travel patterns have been impacted and the collection of turning movement counts would not reflect typical volume conditions within the study area.

For the purposes of this report, Paradigm has referenced historical turning movement counts completed by Traffic Survey Analysis (TSA). TSA completed eight-hour turning movement counts at both intersections on Thursday November 24, 2016. These counts have been factored to a 2022 base year condition by applying a 2.0\% compounded per annum growth rate to through movements only as per Town staff review comments. The use of historical data and the growth rate were previously signed-off on by Town staff during prestudy consultation.

Historical traffic volume data (2009 to 2017) along Regional Road 50 and Mayfield Road were reviewed to verify the use of the $2.0 \%$ growth rate on the Regional roads. The data was obtained from Region of Peel OpenData Portal ${ }^{5}$.

On Regional Road 50, the data indicates a growth rate of $1.1 \%$ and -0.1\% north and south of Albion Vaughan Road/Mayfield Road, respectively, whereas, the Mayfield Road data indicates a growth rate of $0.4 \%$. A conservative approach (i.e., errs on the high side) was adopted by using the same $2.0 \%$ compounded per annum growth rate. Appendix B contains historical data extracted and growth rate calculations for reference.

The 2016 traffic counts at Regional Road 50 and Albion Vaughan Road/Mayfield Road were completed from 6:00 AM to 10:00 AM, and 2:00 PM to 6:00 PM. The counts at Albion Vaughan Road and Kirby Road were completed from 6:00 AM to 9:00 AM, 11:30 AM to 1:30 PM, and from 3:00 PM to 6:00 PM. All traffic movements, including pedestrian crossings were counted in 15-minute intervals and vehicles were classified by type.

Figure 3.2 illustrates the base year (2022) traffic volumes. Appendix C contains the raw count data for reference.

[^3]
### 3.6 Traffic Observations

Based upon notes and observations conducted when the historical counts were collected in November 2016, it was noted that a good level of service was generally provided in the study area.

The exception being that the westbound left-turn movement on Albion Vaughan Road at Regional Road 50 was observed to experience a high level of delay in the AM peak hour.

This observation is further validated by the high volume of vehicles performing the movement. The raw unadjusted 2016 counts recorded 491 vehicles performing this movement exceeding 300 vehicles per hour during the AM peak hour, which is the threshold where both the Highway Capacity Manual and the Transportation Association of Canada Geometric Design Guide for Canadian Roads recommend the consideration of dual left-turn lanes.


## Base Year Traffic Volumes AM Peak Hour



## Base Year Traffic Volumes PM Peak Hour

### 3.7 Traffic Operations

Intersection Level of Service (LOS) is a recognized method of quantifying the efficiency of traffic flow at intersections and is based on the delay experienced by individual vehicles executing the various movements. The delay is related to the number of vehicles desiring to make a movement, compared to the estimated capacity for that movement. The capacity is based on several criteria related to opposing traffic flows, and at signalized intersections, signal timing. Capacity is evaluated in terms of the ratio of demand flow to capacity with an at-capacity condition represented by a volume-to-capacity (v/c) ratio of 1.00 (i.e., volume demand equals capacity).

The highest possible rating is LOS A, under which the average total delay at signalized and unsignalized intersections is equal or less than 10 seconds per vehicle. When the average delay for a movement exceeds 80 seconds at signalized intersections, or 50 seconds at unsignalized intersections, the movement is classified as LOS F, and remedial measures are usually implemented, if they are feasible.

To adhere to the Region of Peel guidelines for operational analysis ${ }^{6}$, the following criteria have been used for the determination of the need for capacity or traffic control improvements to the study area intersections.

- When v/c ratios for overall intersection operations, through movements, or shared through/turning movements exceeds 0.90;
- When v/c ratios for dedicated turning movements exceeds 1.00; and/or
- When $95^{\text {th }}$ percentile queue lengths for individual movements exceeds available lane storage.

To assess the base year traffic operating conditions, a level of service analysis has been conducted using Synchro software, which implements the methods of the Highway Capacity Manual (HCM). The following parameters have been utilized in the analysis:

- Existing lane configurations;
- Signal timing as provided by the Region (and included in Appendix C for reference);
- Heavy vehicles percentages and crossing pedestrian volumes as extracted from the turning movement counts;

[^4]- Lane widths as per "Regional Guidelines for Using Synchro" 7;
- Peak hour factors of 1.00 as per "Regional Guidelines for Using Synchro" ${ }^{\text {8 }}$; and
- Synchro default values for all other inputs.

Table 3.2 presents the operational analysis results including the level of service (LOS), average delay in seconds, volume to capacity (v/c) ratio, and $95^{\text {th }}$ percentile queue length in metres. Any critical movements are highlighted in yellow.

Appendix D contains the Synchro analysis outputs for reference.
In summary, the base year operations represent acceptable levels of service. All traffic movements are currently found to operate acceptably and within capacity.

It is noted the westbound left turn movement is approaching capacity under base year traffic conditions.

The $95^{\text {th }}$ percentile queue lengths were checked for all turn lanes against provided storage, and queue lengths for through movements were also checked. It was confirmed no spillback issues are present.

[^5]TABLE 3.2: BASE YEAR TRAFFIC OPERATIONS

| Intersection | Approach/ Movement |  | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS ${ }^{1}$ | Delay ${ }^{2}$ | V/C ${ }^{3}$ | Q ${ }^{4}$ | LOS ${ }^{1}$ | Delay ${ }^{2}$ | V/C ${ }^{3}$ | Q ${ }^{4}$ |
| Regional Road <br> 50 \& Albion <br> Vaughan <br> Road/Mayfield <br> Road <br> Signalized | EB | Left | D | 55 | 0.51 | 31 | D | 40 | 0.56 | 11 |
|  |  | Thru | E | 64 | 0.59 | 49 | D | 50 | 0.67 | 40 |
|  |  | Right | D | 54 | 0.09 | 16 | D | 38 | 0.07 | 46 |
|  | WB | Left | E | 75 | 0.97 | 165 | D | 45 | 0.65 | 1 |
|  |  | Thru | D | 52 | 0.66 | 94 | D | 44 | 0.47 | 12 |
|  |  | Right | D | 39 | 0.01 | <1 | D | 38 | 0.02 | 16 |
|  | NB | Left | C | 27 | 0.56 | 27 | B | 13 | 0.32 | 3 |
|  |  | Dual Thru | B | 16 | 0.41 | 77 | B | 15 | 0.59 | 20 |
|  |  | Right | B | 13 | 0.10 | 9 | B | 12 | 0.34 | 23 |
|  | SB | Left | C | 20 | 0.01 | 2 | B | 15 | 0.07 | 4 |
|  |  | Dual Thru | D | 36 | 0.79 | 203 | C | 21 | 0.59 | <1 |
|  |  | Right | C | 21 | 0.07 | 11 | B | 15 | 0.09 | $<1$ |
|  | Overall Intersection |  | D | 39 | 0.81 | - | C | 22 | 0.63 | - |
| Albion Vaughan Road \& Kirby Road <br> Unsignalized | WB | Left/Right | C | 18 | 0.12 | 3 | C | 21 | 0.27 | 7 |
|  | NB | Thru/Right | Unopposed Movement |  |  |  | Unopposed Movement |  |  |  |
|  | SB | Left/Thru | A | 2 | 0.09 | 2 | A | 1 | 0.04 | 1 |

## 4 Future Traffic Conditions

### 4.1 Horizon Years

Consistent with the terms of reference established, traffic forecasts have been developed for a period five-years from year of buildout/occupancy.

For assessment purposes it is anticipated the residential development would be built and occupied by 2024; therefore, a horizon year of 2029 will be analyzed.

### 4.2 Forecast Background Traffic

The future background traffic volumes in the study area are expected to comprise general background growth and specific traffic generated by approved or in-stream developments.

During pre-study consultation, Town staff advised the use of a 2.0\% compounded per annum growth rate for application on roadways under the Town's jurisdiction.

We have also applied this growth rate to the Regional roads within the study area. This $2.0 \%$ compounded growth rate represents a conservative approach (i.e., errs on the high side). Detailed discussion can be found in Section 3.5.

As per review comments, this growth rate has been applied to through movements only on the study roadways. Town staff also confirmed there were no background developments to include as part of the traffic forecasts.

Figure illustrates the forecast background traffic volumes for the 2029 horizon year.


## 2029 Background Traffic Volumes AM Peak Hour



## 2029 Background Traffic Volumes PM Peak Hour

### 4.3 Site Trip Generation

### 4.3.1 Vehicle Trip Generation

Trip generation for the subject development has been estimated using information contained in the Institute of Transportation Engineers (ITE) publication, "Trip Generation Manual, $11^{\text {th }}$ Edition" 9 .

Specifically, trip equations for Land Use Code (LUC) 221 - Multifamily Housing (Mid-Rise) were used. This land use is defined as "apartments and condominiums located in a building that has between four and ten floors of living space".

Table summarizes the trip generation estimates and indicates the site is forecast to generate a total of 105 new vehicle trips in the AM peak hour and 104 new vehicle trips in the PM peak hour.

As noted in Section 3.4, trips to and from the study area are predominantly automobile based (accounting for approximately 90\% or higher of all trips); therefore, no adjustments have been made to account for trips made by transit or alternative travel modes.

TABLE 4.1: SITE TRIP GENERATION

| LUC | Units | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rate | In | Out | Total | Rate | In | Out | Total |  |
| 221 | 265 | Eqn. ${ }^{1}$ | 24 | 81 | 105 | Eqn. ${ }^{2}$ | 63 | 41 | 104 |
| Total Trip Generation |  | $\mathbf{2 4}$ | $\mathbf{8 5}$ | $\mathbf{1 0 5}$ |  | 63 | $\mathbf{4 1}$ | $\mathbf{1 0 4}$ |  |

${ }^{1}$ - AM: $\mathrm{T}=0.44(\mathrm{X})-11.61$ ( $23 \%$ inbound, $77 \%$ outbound)
${ }^{2}$ - PM: $\mathrm{T}=0.39(\mathrm{X})+0.34$ ( $61 \%$ inbound, $39 \%$ outbound)

### 4.3.2 Site Trip Distribution and Assignment

Trip distribution for the development site is based on a review of existing traffic patterns and trip distribution data extracted from 2016 Transportation Tomorrow Survey (TTS) data. Table 4.2 and Table 4.3 summarize existing travel patterns based on intersection turning movement count data, and 2016 TTS trip distribution data, respectively.

TTS trip distribution was then combined with existing traffic pattern distributions by estimating by route. Table 4.4 illustrates the estimated site trip distribution. Appendix E details trip distribution calculations.

[^6]TABLE 4.2: EXISTING TRAVEL PATTERN DISTRIBUTION

| Origin/Destination | AM Peak Hour |  | PM Peak Hour |  |
| :--- | :---: | :---: | :---: | :---: |
|  | In | Out | In | Out |
| North via Regional Road 50 | $36 \%$ | $26 \%$ | $30 \%$ | $36 \%$ |
| South via Regional Road 50 | $29 \%$ | $52 \%$ | $48 \%$ | $32 \%$ |
| West via Mayfield Road | $10 \%$ | $14 \%$ | $13 \%$ | $10 \%$ |
| North via Albion Vaughan Road | $\mathbf{2 5 \%}$ | $8 \%$ | $9 \%$ | $22 \%$ |
| Total | $\mathbf{1 0 0 \%}$ | $\mathbf{1 0 0 \%}$ | $\mathbf{1 0 0 \%}$ | $\mathbf{1 0 0 \%}$ |

TABLE 4.3: TTS TRIP DISTRIBUTION

| Origin/Destination | AM Peak Hour |  | PM Peak Hour |  |
| :--- | :---: | :---: | :---: | :---: |
|  | In | Out | In | Out |
| North | $65 \%$ | $44 \%$ | $33 \%$ | $61 \%$ |
| South | $23 \%$ | $50 \%$ | $57 \%$ | $22 \%$ |
| West | $12 \%$ | $6 \%$ | $10 \%$ | $17 \%$ |
| Total | $\mathbf{1 0 0} \%$ | $\mathbf{1 0 0} \%$ | $\mathbf{1 0 0} \%$ | $\mathbf{1 0 0 \%}$ |

TABLE 4.4: ESTIMATED SITE TRIP DISTRIBUTION

| Origin/Destination | AM Peak Hour |  | PM Peak Hour |  |
| :--- | :---: | :---: | :---: | :---: |
|  | In | Out | In | Out |
| North via Regional Road 50 | $38 \%$ | $34 \%$ | $25 \%$ | $38 \%$ |
| South via Regional Road 50 | $23 \%$ | $50 \%$ | $57 \%$ | $22 \%$ |
| West via Mayfield Road | $12 \%$ | $6 \%$ | $10 \%$ | $17 \%$ |
| North via Albion Vaughan Road | $27 \%$ | $10 \%$ | $8 \%$ | $23 \%$ |
| Total | $\mathbf{1 0 0 \%}$ | $\mathbf{1 0 0 \%}$ | $\mathbf{1 0 0 \%}$ | $\mathbf{1 0 0 \%}$ |

The estimated trip generation has been assigned to the study road network based on the distribution noted in Table 4.4. Based on the intended operation of the north and south driveway connections for service and delivery vehicles exclusively, all site traffic has been assigned to the central middle access driveway.

Figure 4.2 illustrates the site-generated vehicle traffic assignment for the AM and PM peak hours. Slight differences from the trip generation estimates are due to rounding.

### 4.4 Forecast Total Traffic

The future background traffic forecasts were combined with the site traffic assignments to estimate the future total traffic volumes for the 2029 horizon year.

Figure 4.3 illustrates the 2029 total traffic forecasts.


## Site Traffic Volumes <br> AM Peak Hour



## Site Traffic Volumes <br> PM Peak Hour



## 2029 Total Traffic Volumes <br> AM Peak Hour



## 2029 Total Traffic Volumes PM Peak Hour

## 5 Transportation Impact Assessment

### 5.1 Future Background Traffic

To assess the operating conditions for the 2029 horizon year, analyses were undertaken using the same methodology, parameters, and traffic control devices as in the analysis of base year conditions.

The exception includes the optimization of timing splits within existing cycle lengths to improve traffic operations for all movements. Table 5.1 presents the signal timing splits at the intersection of Regional Road 50 and Albion Vaughan Road/Mayfield Road for the existing and background conditions.

TABLE 5.1: SIGNAL TIMING SPLITS

| Condition | Phase 1 | Phase 2 | $\begin{gathered} \text { Phase } \\ 3 \\ \hline \end{gathered}$ | Phase 4 | $\begin{gathered} \text { Phase } \\ 6 \end{gathered}$ | Phase <br> 7 | $\begin{gathered} \hline \text { Phase } \\ 8 \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NBL | SBTL | WBL | EBTL | NBTL | EBL | WBTL |
| AM Peak Hour |  |  |  |  |  |  |  |
| Existing | 25 s | 63 s | 27 s | 45 s | 88 s | 10 s | 62 s |
| $\begin{array}{\|l\|} \hline 2029 \\ \text { Background } \\ \hline \end{array}$ | 16 s | 75.5 s | 39 s | 29.5 s | 91.5 s | 10 s | 58.5 s |
| Change | -9 s | $\begin{gathered} +12.5 \\ s \\ \hline \end{gathered}$ | +12 s | $\begin{gathered} -15.5 \\ s \\ \hline \end{gathered}$ | +3.5 s | Nil | -3.5s |
| PM Peak Hour |  |  |  |  |  |  |  |
| Existing | 25 s | 50 s | 10 s | 40 s | 75 s | 10 s | 40 s |
| $\begin{array}{\|l\|} \hline 2029 \\ \text { Background } \\ \hline \end{array}$ | 25 s | 50 s | 10 s | 40 s | 75 s | 10 s | 40 s |
| Change | Nil | Nil | Nil | Nil | Nil | Nil | Nil |

Table 5.2 presents the operational analysis results including level of service (LOS), average vehicle delay in seconds, volume to capacity ( $\mathrm{v} / \mathrm{c}$ ) ratio, and $95^{\text {th }}$ percentile queues length in metres for the 2029 horizon. Critical movements are highlighted in yellow, if any.

Appendix F contains the detailed Synchro reports.
The analysis of background conditions (without the subject development) indicates the study area intersections are forecast to operate at acceptable level of services and within capacity.

The exception would be at the intersection of Regional Road 50 and Albion Vaughan Road/Mayfield Road during the AM peak hour. The following critical movements are reported:

- The overall intersection reports a v/c ratio of 0.95 ; and
- Southbound dual through movement is forecast to operate at LOS D with a v/c ratio of 0.94 .

TABLE 5.2: 2029 BACKGROUND TRAFFIC OPERATIONS

| Intersection | Approach/ Movement |  | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS ${ }^{1}$ | Delay ${ }^{2}$ | V/C ${ }^{3}$ | Q ${ }^{4}$ | LOS ${ }^{1}$ | Delay ${ }^{2}$ | V/C ${ }^{3}$ | Q ${ }^{4}$ |
| Regional Road <br> 50 \& Albion <br> Vaughan <br> Road/Mayfield <br> Road <br> Signalized | EB | Left | E | 64 | 0.55 | 32 | D | 40 | 0.56 | 10 |
|  |  | Thru | E | 77 | 0.69 | 62 | D | 51 | 0.71 | 41 |
|  |  | Right | E | 61 | 0.09 | 17 | D | 38 | 0.07 | 46 |
|  | WB | Left | E | 72 | 0.95 | 153 | D | 46 | 0.67 | 1 |
|  |  | Thru | D | 49 | 0.61 | 111 | D | 44 | 0.50 | 15 |
|  |  | Right | D | 38 | 0.01 | 0 | D | 37 | 0.02 | 19 |
|  | NB | Left | E | 76 | 0.80 | 51 | B | 17 | 0.39 | 4 |
|  |  | Dual Thru | C | 23 | 0.50 | 108 | B | 18 | 0.70 | 24 |
|  |  | Right | B | 17 | 0.10 | 10 | B | 13 | 0.36 | 27 |
|  | SB | Left | C | 24 | 0.01 | 2 | B | 17 | 0.10 | 4 |
|  |  | Dual Thru | D | 54 | 0.94 | 256 | C | 25 | 0.69 | <1 |
|  |  | Right | C | 25 | 0.07 | 11 | B | 16 | 0.09 | $<1$ |
|  | Overall Intersection |  | D | 48 | 0.95 | - | C | 25 | 0.72 | - |
| Albion Vaughan Road \& Kirby Road <br> Unsignalized | WB | Left/Right | C | 21 | 0.14 | 4 | D | 27 | 0.33 | 10 |
|  | NB | Thru/Right | Unopposed Movement |  |  |  | Unopposed Movement |  |  |  |
|  | SB | Left/Thru | A | 3 | 0.10 | 2 | A | 1 | 0.05 | 1 |

### 5.2 Future Total Traffic

To assess operating conditions for the future total forecasts, an operational analysis was undertaken using the same methodology, parameters, and traffic control devices as in the analysis of background conditions.

Table 5.3 presents the operational analysis results including level of service (LOS), average vehicle delay in seconds, volume to capacity (v/c) ratio, and $95^{\text {th }}$ percentile queues length in metres for the 2029 horizon. Critical movements are highlighted in yellow, if any.

Appendix G contains the detailed Synchro reports.
The analysis of total conditions (with the subject development) indicates the study area intersections would continue to operate at acceptable conditions, albeit slightly exacerbated with the inclusion of site-generated traffic.

The previously identified critical movements under background conditions would continue to be reported, albeit slightly exacerbated under total conditions. No additional critical movements were identified.

The site access intersection with Albion Vaughan Road is noted to operate at good levels of service and well within capacity.

TABLE 5.3: 2029 TOTAL TRAFFIC OPERATIONS

| Intersection | Approach/ <br> Movement |  |  | AM Peak Hour $^{2}$ |  |  |  | LOS $^{1}$ | Delay $^{2}$ | V/C $^{3}$ | Q $^{4}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Delay |  |  |  |  |  |  |  |  |  |  |

### 5.3 Impact Assessment Summary

### 5.3.1 Site Traffic

Overall, the incremental impact of the proposed residential development is considered minor. The additional traffic would be less than daily traffic variations typically experienced (approximately 10\%).

Table 5.4 provides a summary of how much traffic volumes will increase by with the subject residential development.

TABLE 5.4: TRAFFIC VOLUME INCREASE

| Intersection | 2029 Background vs. 2029 Total <br> \% Volume Increase (Total Entering) |  |
| :--- | :---: | :---: |
|  | AM Peak Hour | PM Peak Hour |
|  <br> Albion Vaughan Road/Mayfield <br> Road | $2.3 \%$ | $2.2 \%$ |
| Albion Vaughan Road \& Kirby <br> Road | $1.0 \%$ | $1.1 \%$ |

Under the 2029 background conditions, the intersection of Regional Road 50 and Albion Vaughan Road/Mayfield Road is reported to operate approaching capacity (with an overall v/c of 0.95). The southbound dual through movement is forecast to operate with a v/c of 0.94 . The same critical movements were identified under 2029 total conditions.

With employers beginning to shift away from traditional office-based environments to work-from-home models and with commercial/retail and service-based businesses adapting by adjusting business hours and/or switching to web-based e-commerce storefronts, travel demands and patterns are changing.

In a post-COVID condition, it is plausible that traffic volumes may never reach pre-COVID levels as a result of this quantum shift that is being experienced. With changes in travel demand, behaviour, and patterns post-COVID due to changes in how office and business environments operate. The forecasts as analyzed are conservative and potentially under post-COVID conditions, traffic volumes may be considerably lower than forecast if the forecast growth is not materialized.

### 5.3.2 Intersection Improvements

Regional Road 50 and Albion Vaughan Road/Mayfield Road

Dual left-turn lanes for the westbound approach have been investigated as a potential mitigation measure to improve the overall intersection operations and the westbound left turn movement. While the movement has not been identified as a critical movement, from a volume perspective the movement would warrant the consideration of a dual left-turn lanes.

The westbound left-turn traffic volume is reported as 491 and 534 vehicles during the AM peak hour under the 2029 background and total traffic conditions, respectively. The amount of left-turn traffic exceeds the 300 vehicles per hour threshold identified by both the Highway Capacity Manual and the Transportation Association of Canada Geometric Design Guide for Canadian Roads for the consideration of dual left-turn lanes.

The following signal timing plan changes are proposed to provide the best possible traffic operations for all movements in the event that westbound dual left-turn lanes are implemented.

- The westbound left-turn movement turn type shall be changed from permitted/protected to a fully-protected movement; and
- Optimization of signal timing splits within the existing cycle lengths.

Table 5.5 presents the proposed signal timing split changes for the AM peak hour for the existing, background and total conditions.

TABLE 5.5: SIGNAL TIMING SPLITS - WB DUAL LEFT-TURN LANES

| Condition | Phase 1 | Phase 2 | $\begin{gathered} \text { Phase } \\ 3 \\ \hline \end{gathered}$ | Phase $4$ | $\begin{gathered} \text { Phase } \\ 6 \\ \hline \end{gathered}$ | Phase $7$ | $\begin{gathered} \text { Phase } \\ 8 \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NBL | SBTL | WBL | EBTL | NBTL | EBL | WBTL |
| AM Peak Hour |  |  |  |  |  |  |  |
| Existing | 25 s | 63 s | 27 s | 45 s | 88 s | 10 s | 62 s |
| $\begin{array}{\|l\|} \hline 2029 \\ \text { Background } \\ \hline \end{array}$ | 16 s | 76 s | 28.5 s | 39.5 s | 92 s | 11.5 s | 56.5 s |
| 2029 Total | 16 s | 76 s | 29 s | 39 s | 92 s | 10 s | 58 s |
| PM Peak Hour |  |  |  |  |  |  |  |
| Existing | 25 s | 50 s | 10 s | 40 s | 75 s | 10 s | 40 s |
| $\begin{array}{\|l\|} \hline 2029 \\ \text { Background } \\ \hline \end{array}$ | 11 s | 60.4 s | 14 s | 39.6 s | 71.4 s | 13 s | 40.6 s |
| 2029 Total | 11 s | 60.4 s | 14 s | 39.6 s | 71.4 s | 13 s | 40.6 s |

Table 5.6 and Table 5.7 present the results of the operational analysis at the intersection of Regional Road 50 and Albion Vaughan Road/Mayfield Road for the 2029 background and total traffic conditions, respectively with the implementation of westbound dual leftturn lanes. Appendix H contains the Synchro analysis outputs for reference.

With the provision of dual left-turn lanes on the westbound approach, the intersection is reported to operate at acceptable levels of service and with all movements within capacity. No more critical movements are identified.

TABLE 5.6: 2029 BACKGROUND TRAFFIC OPERATIONS - DUAL LEFT-TURN LANES

| Intersection | Approach/ Movement |  | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS ${ }^{1}$ | Delay ${ }^{2}$ | V/C ${ }^{3}$ | Q ${ }^{4}$ | LOS ${ }^{1}$ | Delay ${ }^{2}$ | V/C ${ }^{3}$ | Q ${ }^{4}$ |
| Regional Road 50 \& Albion Vaughan Road/Mayfield Road <br> Signalized | EB | Left | D | 55 | 0.49 | 32 | C | 35 | 0.48 | 41 |
|  |  | Thru | E | 68 | 0.63 | 57 | D | 51 | 0.71 | 73 |
|  |  | Right | E | 56 | 0.09 | 16 | D | 38 | 0.07 | 11 |
|  | WB | Dual Left | E | 71 | 0.83 | 97 | D | 54 | 0.53 | 29 |
|  |  | Thru | E | 59 | 0.75 | 114 | D | 43 | 0.48 | 49 |
|  |  | Right | D | 41 | 0.01 | <1 | D | 37 | 0.02 | <1 |
|  | NB | Left | E | 59 | 0.74 | 47 | C | 21 | 0.47 | 14 |
|  |  | Dual Thru | B | 19 | 0.47 | 101 | C | 21 | 0.74 | 161 |
|  |  | Right | B | 14 | 0.10 | 10 | B | 15 | 0.34 | 16 |
|  | SB | Left | C | 21 | 0.01 | 2 | B | 19 | 0.11 | 6 |
|  |  | Dual Thru | D | 42 | 0.87 | 242 | C | 26 | 0.71 | 145 |
|  |  | Right | C | 21 | 0.07 | 10 | B | 16 | 0.09 | 11 |
|  | Overall Intersection |  | D | 42 | 0.85 | - | C | 26 | 0.73 | - |

TABLE 5.7: 2029 TOTAL TRAFFIC OPERATIONS - DUAL LEFT-TURN LANES

| Intersection | Approach/ Movement |  | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS ${ }^{1}$ | Delay ${ }^{2}$ | V/C ${ }^{3}$ | Q ${ }^{4}$ | LOS ${ }^{1}$ | Delay ${ }^{2}$ | V/C ${ }^{3}$ | $\mathrm{Q}^{4}$ |
| Regional Road 50 \& Albion Vaughan Road/Mayfield Road | EB | Left | E | 57 | 0.52 | 32 | C | 35 | 0.48 | 40 |
|  |  | Thru | E | 69 | 0.65 | 59 | D | 51 | 0.72 | 75 |
|  |  | Right | E | 57 | 0.09 | 16 | D | 38 | 0.07 | 11 |
|  | WB | Dual Left | E | 74 | 0.88 | 108 | D | 54 | 0.56 | 30 |
|  |  | Thru | E | 56 | 0.72 | 114 | D | 43 | 0.50 | 51 |
|  |  | Right | D | 40 | 0.03 | 4 | D | 37 | 0.04 | 2 |
|  | NB | Left | E | 60 | 0.74 | 47 | C | 21 | 0.48 | 14 |
|  |  | Dual Thru | B | 19 | 0.47 | 100 | C | 22 | 0.74 | 162 |
| Signalized |  | Right | B | 14 | 0.11 | 10 | B | 16 | 0.39 | 24 |
|  | SB | Left | C | 22 | 0.06 | 6 | C | 26 | 0.29 | 13 |
|  |  | Dual Thru | D | 42 | 0.88 | 233 | C | 26 | 0.71 | 145 |
|  |  | Right | C | 21 | 0.07 | 10 | B | 17 | 0.09 | 11 |
|  | Overall Intersection |  | D | 43 | 0.85 | - | C | 27 | 0.73 | - |

## Albion Vaughan Road and Site Access

From an operational standpoint, auxiliary turn lanes on Albion Vaughan Road are not necessary as the shared northbound left/through movement and the shared southbound through/right movements are both are reported to operate at LOS A and the movements are forecast to be well within capacity.

Regardless, the warrants for left-turn lanes within the Ontario Ministry of Transportation's (MTO) Design Supplement to the TAC Geometric Design Guide for Canadian Roads (TAC Guide) were investigated. The warrant is based on a combination of the advancing and opposing design hour volumes, the design speed of the road, and the percentage of left-turning vehicles in the advancing volume.

A warrant analysis has been completed using the nomographs for twolane, unsignalized intersections, with a design speed of $80 \mathrm{~km} / \mathrm{h}(20$ $\mathrm{km} / \mathrm{h}$ over the posted speed limit). Table 5.8 summarizes the details of the left-turn warrant analysis.

TABLE 5.8: LEFT-TURN LANE WARRANT ANALYSIS

| Major Street | Albion Vaughan Road |  |  |
| :--- | :---: | :---: | :---: |
| Minor Street | Site Access |  |  |
| Approach Direction | Northbound |  |  |
| Design Speed | AM | km/h |  |
| Peak Hour | 319 | 995 |  |
| Advancing Volume | 951 | 382 |  |
| Opposing Volume | 17 | 58 |  |
| Left-Turn Volume | $5 \%$ | $6 \%$ |  |
| $\%$ Left Turns | Yes | Yes |  |
| Warranted |  |  |  |

Based upon 2029 total traffic forecasts, a northbound auxiliary left-turn lane is determined to be warranted from a volume perspective.

However, aforementioned, from an operational perspective it is noted that the shared northbound left/through movement is reported to operate at LOS A and the movement is forecast to be well within capacity.

Based upon the low forecast volume of southbound right-turn volumes, it is determined an auxiliary right-turn lane would not be necessary. As the forecast volume of turning traffic is low, it is anticipated these vehicles will not impede southbound traffic on Albion Vaughan Road or cause any undue hazard to through traffic.

In summary, a northbound auxiliary left-turn lane and southbound auxiliary right-turn lane at the site access is not recommended as determined from the traffic operational analysis, the noted movements would operate with minimal delay and well within capacity. Furthermore, the reported $95^{\text {th }}$ percentile queues at the site access are not anticipated to encroach or spill back to adjacent intersections.

## 6 Parking Review

### 6.1 Development Overview

The proposed residential development comprises two residential towers, with a total of 265 residential dwelling units. The development statistics are as follows:

- One six-storey residential tower with 114 units total:
- 37 one-bedroom units;
- 22 one-bedroom + den units;
- 31 two-bedroom units;
- 18 two-bedroom + large balcony units;
- 6 three-bedroom units.
- One seven-storey residential tower with 151 units total:
- 41 one-bedroom units;
- 14 one-bedroom + den units;
- 68 two-bedroom units;
- 21 two-bedroom + large balcony units;
- 7 three-bedroom units.

A total of 462 parking spaces serving residents and visitors are proposed on-site, including 12 accessible parking spaces. The parking supply breakdown is as follows:

- 10 spaces at-grade;
- 221 spaces on parking level P1; and
- 231 spaces on parking level P2.


### 6.2 Zoning By-law Parking Requirements

Table 6.1 presents a comparison of the required and proposed number of vehicle parking spaces under the Town of Caledon Zoning By-law, Section 5: Parking, Loading and Delivery Standards ${ }^{10}$.

The proposed vehicle parking supply does not meet the Town's By-law requirements and results in a theoretical deficit of 2 parking spaces.

[^7]Specifically, the development is proposing to satisfy the visitor parking requirement, and is seeking a $0.5 \%$ reduction in the resident parking component (rate of 1.49 spaces/unit vs. 1.50 spaces/unit).

TABLE 6.1: REQUIRED AND PROVIDED PARKING

| Type of <br> Use | By-law <br> Requirement | Required | Provided | Net Surplus <br> (Deficiency) |
| :---: | :---: | :---: | :---: | :---: |
|  | 1.5 spaces per <br> dwelling unit for <br> residents | 398 | 396 | -2 |
| Apartment <br> (265 units) | 0.25 spaces <br> per unit for <br> visitors | 66 | 66 | - |
|  | $\mathbf{4 6 4}$ | $\mathbf{4 6 2}$ | $\mathbf{- 2}$ |  |

### 6.3 Accessible Parking Requirements

The accessible parking requirements for the subject site have been verified against the Town of Caledon Zoning By-law 2015-58, Schedule K: Designed Accessible Parking Spaces ${ }^{11}$.

The minimum number of accessible parking spaces is two accessible spaces plus $2 \%$ of the proposed parking spaces, when the required number of parking spaces is between 201 and 1000.

Table 6.2 presents a comparison of the required and proposed number of accessible parking spaces. The proposed accessible parking supply for the residential development meets and satisfies the Town's By-law requirements with a surplus of one accessible parking space.

TABLE 6.2: REQUIRED AND PROVIDED ACCESSIBLE PARKING
$\begin{array}{|c|c|c|c|c|}\hline \begin{array}{c}\text { Proposed } \\ \text { Parking } \\ \text { Supply }\end{array} & \begin{array}{c}\text { By-law } \\ \text { Requirement }\end{array} & \text { Required } & \text { Provided } & \begin{array}{c}\text { Net Surplus } \\ \text { (Deficiency) }\end{array} \\$\cline { 4 - 5 } \& 2 spaces + 2\% <br> of total\end{array}$)$

[^8]
### 6.4 Parking Justification

In our professional opinion, the resultant resident component deficiency of 2 spaces is considered acceptable for the proposed development. The rationale and justification is as follows:

- The proposed resident parking supply represents a $0.5 \%$ reduction from the Town's municipal requirement. A rate of 1.49 spaces/unit is proposed in comparison to the requirement of 1.50 spaces/unit.

Based upon a policy review of adjacent neighbouring municipalities, in the City of Vaughan and in the City of Mississauga, a relatively minor parking reduction is considered to be $10 \%$ or less of the By-law requirements per their parking study guidelines;

- Institute of Transportation Engineers (ITE) Parking Generation $5^{\text {th }}$ Edition data was referenced which further supports the proposed resident parking rate.

For LUC 221, the forecast peak parking demand for 265 dwelling units is 347 based upon the both the fitted curve and average rate. The forecast demand is less than the proposed resident supply of 398 space, resulting in a potential surplus of 51 parking spaces. Appendix C contains the ITE data for reference;

- While the subject site is served by limited transit service and active transportation infrastructure, it is anticipated that prospective residents will continue to travel to and from the site via automobile.

However, with parking for the development to be unbundled from residential units. That is, parking spaces are to be rented/sold separately from the dwelling units. Prospective residents may choose not to own a vehicle or opt to forego their vehicle based upon as they see fit.

Overall, there will be a self-regulating process where building residents with cars will favour units where parking is readily available, and those without cars will tend to choose units without regard to the parking provisions/arrangements.

Therefore, prospective unit buyers or renters will either choose to live in this building or not to if parking is or is not available based upon their needs;

- With recent paradigm shifts occurring in work environments. Typical in-person models have been shifting towards remote work-from-home models. As a result of increased work from
home opportunities, average vehicle ownership rates have decreased from an anecdotal standpoint;
- The provision of on-site long-term and short-term bicycle parking to encourage and promote alternative travel modes to the automobile;
- A reduced parking supply is in line with smart growth policies; and
- The development and implementation of a Transportation Demand Management (TDM) Plan will assist in reducing single occupancy vehicle (SOV) trips and the associated parking demands.


### 6.5 Summary

Based on the information presented above, the proposed parking supply is considered to be sufficient in serving the proposed residential development.

In summary the proposed 2 resident component parking space deficiency is not determined to be a critical issue. The proposed $0.5 \%$ reduction in resident supply is considered minor.

At a minimum, 1.49 parking spaces will be provided for each dwelling unit. Prospective residents of this building will effectively operate on a self-regulation basis determined by available parking as resident parking spaces will be unbundled from each dwelling unit.

The proposed resident supply of 396 spaces is supported by ITE Parking Generation demand data. The 265 dwelling units are forecast to generate a peak parking demand of 347 spaces, resulting in a surplus of 51 spaces.

As the visitor parking requirements will be met, it is not anticipated that there will be any undue impact on the Township or the adjacent neighbourhoods.

## 7 Circulation Review

AutoTURN software was used to review and confirm that design of the site accesses, internal circulation, and loading areas will accommodate the types of vehicles expected on-site. This involved the following tasks:

- Showing how a Region of Peel waste collection vehicle would enter the site, access the loading spaces, and exit the site;
- Showing how a Pumper Fire Truck would enter the site, circulate the designated fire route, and exit the site;
- Showing how a TAC Medium Single-Unit (MSU) truck (design vehicle representing typical service and delivery truck) would enter the site, access the loading spaces, and exit the site; and
- Showing how a TAC Passenger Car (design vehicle representing a large car) would enter the site, circulate, access the underground parking structure, and exit the site.

Our review of the underground parking levels noted that all parking spaces and drive aisle widths meet zoning requirements. Furthermore, no dead-end drive aisles were noted and no parking spaces were flagged to have ingress or egress issues.

Each of the design vehicle manoeuvres described above are accommodated by the design of the site without issue or conflict.

Appendix I contains the vehicle maneuvering diagrams for reference.

## 8 Conclusions and Recommendations

### 8.1 Conclusions

The conclusions of the study are as follows:

- Under the base year conditions, all study area intersections operate at acceptable levels of service and within capacity.
- For the 2029 background traffic conditions (without subject development), all study area intersections are forecast to operate at acceptable levels of service and within capacity.

The exception would be the Regional Road 50 and Albion Vaughan Road/Mayfield Road intersection, where the overall intersection $\mathrm{v} / \mathrm{c}$ ratio is forecast to be 0.95 during the AM peak hour. The southbound dual through movement is reported to operate with a v/c of 0.94 during the AM peak hour.

- Under the 2029 total traffic conditions (with subject development), all study area intersections are forecast to operate at acceptable levels of service and within capacity.
The previously identified critical movements would continue to be reported, albeit slightly exacerbated.
- The overall impact of the proposed residential development is anticipated to be minimal. The development is estimated to generate and add a total of 105 and 104 vehicle trips to the adjacent transportation network during the AM and PM peak hours, respectively.

The additional traffic would be less than daily traffic variations typically experienced. It is determined the site generated traffic would increase volumes at the study area intersections between 1.0 to $2.3 \%$.

While not identified as a critical movement, auxiliary dual leftturn lanes were investigated at the westbound approach at the intersection of Regional Road 50 and Albion Vaughan Road/Mayfield Road intersection. The movement is acknowledged to be approaching capacity under 2029 background and total traffic conditions.

As analyzed with dual left-turn lanes on the westbound approach and optimization of signal timing splits within exiting cycle lengths, the overall intersection is reported to operate at acceptable levels of service and with all movements within capacity under the 2029 horizon.

- At the main central site access intersection with Albion Vaughan Road, it was determined an auxiliary northbound left-turn lane
would be warranted from a volume perspective. It is noted that the auxiliary left-turn lane is not required from an operational standpoint.
- The proposed overall parking results in a theoretical deficient of 2 spaces in comparison to the minimum zoning by-law requirements. That is, the visitor parking requirements would be satisfied; however, the proposed resident parking requirements would be theoretically deficient by $0.5 \%$.
The proposed resident parking supply is anticipated to adequately serve the residential development. The main basis in support of the minor reduction is supported by ITE Parking Generation forecasts of peak parking demands. The proposed resident supply would result in a surplus of parking based upon the forecast peak demands. Additionally, parking spaces will be unbundled from residential units.
- A review of the site plan was undertaken. No major conflicts or issues were identified for the anticipated design vehicles expected on-site.


### 8.2 Recommendations

The recommendations of the study are as follows:

- From a transportation perspective, the planning applications sought should be approved as the development is determined to have a minimal impact on the adjacent transportation network.
- The intersection volumes and operations at the Regional Road 50 and Albion Vaughan Road/Mayfield Road intersection be monitored by the applicable jurisdiction to determine when dual westbound left-turn lanes should be provided.
- Regardless of being warranted, a northbound auxiliary left-turn lane is not required at the central site access intersection on Albion Vaughan Road based upon forecast traffic operations.


## Appendix A

## Pre-Study Consultation Correspondence

## Adrian Soo

From:
Arash Olia [Arash.Olia@caledon.ca](mailto:Arash.Olia@caledon.ca)
Sent: October 23, 2020 11:14 AM
To: Andrew Steinsky; catherine.barnes@peelregion.ca
Cc: Adrian Soo
Subject:
RE: 200428-12148 Albion Vaughan Road TIS Scope of Work

Hi Andrew,

Please see my comments below in red.

Thanks,

Arash Olia, Ph.D., P.Eng.

Manager, Transportation Engineering
Finance \& Infrastructure Services
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Email: arash.olia@caledon.ca

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From: Andrew Steinsky [asteinsky@ptsl.com](mailto:asteinsky@ptsl.com)
Sent: Thursday, October 22, 2020 10:45 AM
To: catherine.barnes@peelregion.ca; Arash Olia [Arash.Olia@caledon.ca](mailto:Arash.Olia@caledon.ca)
Cc: Adrian Soo [asoo@ptsl.com](mailto:asoo@ptsl.com)
Subject: 200428-12148 Albion Vaughan Road TIS Scope of Work

CAUTION: This email originated from outside of the organization. Do not click links or open attachments unless you recognize the sender and know the contents to be safe.
Hi Arash \& Catherine,
We've been retained to prepare a Traffic Impact Study (TIS) for a residential development on the west side of Albion Vaughan Road, south of Kirby Road in Bolton. We're reaching out to both the Region and Town to confirm our scope of work. If you are not the correct point of contact, please let us know so we can contact the correct person. We would appreciate any comments by the week of November 2.

The development proposal includes 240 condominiums in a six-storey building, and 10 townhomes. Access is proposed through a new all-moves driveway connection to Albion Vaughan Road. Two separate driveway connections for loading and delivery vehicles are also proposed on the north and south edges of the site.

Based on the above, we propose the following work plan to carry out the TIS:

1. Analysis of $A M$ and $P M$ peak hours.
2. Horizon year five years from date of study (2025). Please confirm. From completion/built out date
3. Study area to include:

- Highway 50 \& Mayfield Road/Albion Vaughan Road; and
- Albion Vaughan Road \& Kirby Road.

We have turning movements completed at both intersections on Thursday November 24, 2016. Are these counts acceptable given the current impacts of COVID-19 on traffic volumes? Please confirm an appropriate growth rate to factor these volumes to a 2020 base year. I suggest adopt 2\%
4. Background traffic to be forecast using a per annum growth rate. Please confirm appropriate growth rate. 2\%
5. Background developments to be included? Please confirm. No background development
6. ITE Trip Generation Manual ( $10^{\text {th }}$ Edition) rates to establish trip generation
7. Mode share based on TTS.
8. Trip distribution derived from turning movement counts and origin/destination information obtained from TTS.
9. AutoTURN assessment to include relevant design vehicles expected on the site, and swept path analysis.

Please let me and Adrian Soo (cc'd on this e-mail) if you have any questions on the above work plan.
Thanks,

## Andrew Steinsky, P.Eng.

Transportation Engineer

## paradigm

## Paradigm Transportation Solutions Limited

5A-150 Pinebush Road, Cambridge ON N1R 8J8
p: 416.479.9684 $\times 507$
e: asteinsky@ptsl.com
w: www.ptsl.com
Since 1998, our unique "work at home" business model has enabled us to harness technology, offer high quality service and strong communication with our clients and now allows us to carry on our work for you during COVID-19.

Let's stay safe and look out for each other. We will get through this together.

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## Appendix B <br> Growth Rate Calculation Based on Historical Traffic Volume Data



Task: Growth Rate Calculation

HIGHWAY 50, 1.0 km north of mayfield road

| NE | Volume | SW | Volume | Total |
| :---: | :---: | :---: | :---: | :---: |
| Y_2009_NE | 16325 | Y_2009_SW | 15690 | 32015 |
| Y_2011_NE | 13700 | Y_2011_SW | 13133 | 26833 |
| Y_2012_NE | 14784 | Y_2012_SW | 14130 | 28914 |
| Y_2013_NE | 16816 | Y_2013_SW | 15887 | 32703 |
| Y_2014_NE | 16719 | Y_2014_SW | 15954 | 32673 |
| Y_2015_NE | 17803 | Y_2015_SW | 16408 | 34211 |

Growth Rate $\quad 1.45 \% \quad 0.75 \% \quad 1.11 \%$

HIGHWAY 50, 0.5 km north of countryside/nashville

| NE | Volume | SW | Volume | Total |
| :---: | :---: | :---: | :---: | :---: |
| Y 2011 NE | 12065 | Y 2011 SW | 12029 | 24094 |
| Y 2012 NE | 12100 | Y 2012 SW | 0 | 12100 |
| Y 2013_NE | 15333 | Y 2013 SW | 13319 | 28652 |
| Y 2014 NE | 13552 | Y 2014 SW | 14574 | 28126 |
| Y_2015_NE | 14835 | Y_2015_SW | 14804 | 29639 |
| Y_2016_NE | 16860 | Y_2016_SW | 16767 | 33627 |
| Y_2017_NE | 10860 | Y_2017_SW | 13040 | 23900 |

Mayfield Road, 0.8 km west of hwy 50

| NE | Volume | SW | Volume | Total |
| :---: | :---: | :---: | :---: | :---: |
| Y_2012_NE | 5266 | Y_2012_SW | 5232 | 10498 |
| Y_2013_NE | 5067 | Y_2013_SW | 5054 | 10121 |
| Y_2014_NE | 5451 | Y_2014_SW | 4960 | 10411 |
| Y_2015_NE | 4324 | Y_2015_SW | 4203 | 8527 |
| Y_2016_NE | 0 | Y_2016_SW | 0 | 0 |
| Y_2017_NE | 5542 | Y_2017_SW | 5181 | 10723 |

## Appendix C

## Traffic Data










## Albion Vaughan Road \& Kirby Road Traffic Count Summary

| Intersection: Albion Vaughan Road \& Kirby Roa |  |  |  |  | Count Date: $24-$ Nov-2016 |  | 16 Muni | Municipality: Nobleton |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North Approach Totals |  |  |  |  |  | North/South Total Approaches | South Approach Totals |  |  |  |  |  |
| Hour Ending | Includes Cars, Trucks, \& Heavys |  |  |  | Total |  | Hour Ending | Includes Cars, Trucks, \& Heavys |  |  |  | Total |
|  | Left | Thru | Right | Grand Total |  |  |  | Left | Thru | Right | Grand Total |  |
| 6:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 6:00:00 | 0 | 0 | 0 | 0 | 0 |
| 7:00:00 | 41 | 549 | 0 | 590 | 0 | 764 | 7:00:00 | 0 | 168 | 6 | 174 | 0 |
| 8:00:00 | 128 | 732 | 0 | 860 | 0 | 1075 | 8:00:00 | 0 | 207 | 8 | 215 | 0 |
| 9:00:00 | 69 | 612 | 0 | 681 | 0 | 885 | 9:00:00 | 0 | 198 | 6 | 204 | 0 |
| 12:00:00 | 13 | 95 | 0 | 108 | 0 | 206 | 12:00:00 | 0 | 90 | 8 | 98 | 0 |
| 13:00:00 | 39 | 209 | 0 | 248 | 0 | 462 | 13:00:00 | 0 | 207 | 7 | 214 | 0 |
| 15:00:00 | 21 | 119 | 0 | 140 | 0 | 247 | 15:00:00 | 0 | 101 | 6 | 107 | 0 |
| 16:00:00 | 29 | 272 | 0 | 301 | 0 | 796 | 16:00:00 | 0 | 491 | 4 | 495 | 0 |
| 17:00:00 | 35 | 287 | 0 | 322 | 0 | 980 | 17:00:00 | 0 | 653 | 5 | 658 | 0 |
| 18:00:00 | 26 | 267 | 0 | 293 | 0 | 997 | 18:00:00 | 0 | 692 | 12 | 704 | 0 |
| Totals: | 401 | 3142 | 0 | 3543 | 0 | 6412 |  | 0 | 2807 | 62 | 2869 | 0 |
| East Approach Totals |  |  |  |  |  | East/West Total Approaches | West Approach Totals |  |  |  |  |  |
| Hour Ending | Left | Cars, T | cks, \& H | avys | Total Peds |  | Hour Ending | Left | Cars, T | cks, \& H | avys | Total Peds |
|  |  | Thru | Right | Grand Total |  |  |  |  | Thru | Right | Grand Total |  |
| 6:00:00 | 0 | 0 | 0 | 0 | 0000000010 | 0 | 6:00:00 | $\begin{array}{ll}0 \\ 0 \\ 0 & \\ 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 \\ 0\end{array}$ |  | (1) $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0\end{aligned}$ | 0 | $\begin{array}{ll}0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 \\ 0\end{array}$ |
| 7:00:00 | 2 | 0 | 9 | 11 |  | 11 | 7:00:00 |  |  | 0 |  |
| 8:00:00 | 8 | 0 | 23 | 31 |  | 31 | 8:00:00 |  |  | 0 |  |
| 9:00:00 | 7 | 0 | 29 | 36 |  | 36 | 9:00:00 |  |  | 0 |  |
| 12:00:00 | 3 | 0 | 13 | 16 |  | 16 | 12:00:00 |  |  | 0 |  |
| 13:00:00 | 6 | 0 | 26 | 32 |  | 32 | 13:00:00 |  |  | 0 |  |
| 15:00:00 | 5 | 0 | 7 | 12 |  | 12 | 15:00:00 |  |  | 0 |  |
| 16:00:00 | 12 | 0 | 64 | 76 |  | 76 | 16:00:00 |  |  | 0 |  |
| 17:00:00 | 13 | 0 | 55 | 68 |  | 68 | 17:00:00 |  |  | 0 |  |
| 18:00:00 | 17 | 0 | 56 | 73 |  | 73 | 18:00:00 |  |  | 0 |  |
| Totals: | 73 | 0 | 282 | 355 |  | 355 |  |  |  | 0 |  |
| Calculated Values for Traffic Crossing Major Street |  |  |  |  |  |  |  |  |  |  |  |  |
| Hours En | ing: | 7:00 | 8:00 | 9:00 | 13:00 |  | 15:00 | 16:00 | 17:00 |  | 18:00 |  |  |
| Crossing | Values: | 2 | 8 | 7 | 6 |  | 5 | 12 | 13 |  | 17 |  |  |



## Appendix D

## Base Year Traffic Operations Reports

Lanes，Volumes，Timings

| 1：Regi |  |  |  |  |  |  |  |  |  | Base Yea | ：AM P | k Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 |  |  | $t$ | $\leftarrow$ |  |  | $\dagger$ |  |  | $\dagger$ |  |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ¢ | $\uparrow$ | F | \％ | $\uparrow$ | 「 | ${ }^{7}$ | 个个 | F | ${ }^{7}$ | $\uparrow \uparrow$ | 7 |
| Traffic Volume（vph） | 103 | 123 | 103 | 491 | 287 | 15 | 104 | 813 | 148 | 2 | 1224 | 103 |
| Future Volume（vph） | 103 | 123 | 103 | 491 | 287 | 15 | 104 | 813 | 148 | 2 | 1224 | 103 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 |
| Storage Length（ m ） | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 150.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  |  |
| Taper Length（ m ） | 60.0 |  |  | 40.0 |  |  | 20.0 |  |  | 0.0 |  |  |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Fit |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1580 | 1642 | 1094 | 1767 | 1762 | 1331 | 1214 | 3411 | 1426 | 1190 | 3380 | 1465 |
| Fit Permitted | 0.584 |  |  | 0.598 |  |  | 0.098 |  |  | 0.345 |  |  |
| Satd．Flow（perm） | 971 | 1642 | 1094 | 1112 | 1762 | 1331 | 125 | 3411 | 1426 | 432 | 3380 | 1465 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 103 |  |  | 65 |  |  | 148 |  |  | 103 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance（ m ） |  | 289.2 |  |  | 563.9 |  |  | 378.1 |  |  | 686.1 |  |
| Travel Time（s） |  | 17.4 |  |  | 33.8 |  |  | 19.4 |  |  | 35.3 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles（\％） | 13\％ | 17\％ | 46\％ | 1\％ | 9\％ | 20\％ | 47\％ | 7\％ | 12\％ | 50\％ | 8\％ | 9\％ |
| Adj．Flow（vph） | 103 | 123 | 103 | 491 | 287 | 15 | 104 | 813 | 148 | 2 | 1224 | 103 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 103 | 123 | 103 | 491 | 287 | 15 | 104 | 813 | 148 | 2 | 1224 | 103 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width（ m ） |  | 3.5 |  |  | 3.5 |  |  | 3.5 |  |  | 3.5 |  |
| Link Offset（m） |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Crosswalk Width（m） |  | 4.8 |  |  | 4.8 |  |  | 4.8 |  |  | 4.8 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  | Yes |  |
| Headway Factor | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 |
| Turning Speed（kh） | 25 |  | 15 | 25 |  | 15 | 25 |  | 15 | 25 |  | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 |  |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector（ m ） | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector（m） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position（m） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size（m） | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex | Cl＋Ex |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position（m） |  | 9.4 |  |  | 9.4 |  |  | 9.4 |  |  | 9.4 |  |
| Detector 2 Size（m） |  | 0.6 |  |  | 0.6 |  |  | 0.6 |  |  | 0.6 |  |
| Detector 2 Type |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |  | Cl＋Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend（s） |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm | Perm | NA | Perm |

Lanes，Volumes，Timings

1：Regional Road 50 \＆Mayfield Road／Albion Vaughan Road Base Year：AM Peak Hour | Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Protected Phases | 7 | 4 |  | 3 | 8 | 8 | 1 | 6 |  | 2 | 2 | 2 |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 | Switch Phase

| Minimum Initial（s） | 5.0 | 12.0 | 12.0 | 5.0 | 12.0 | 12.0 | 5.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | 8.0 | 30.0 | 20.5 | 0.0 | 30.0 | 3.5 | 2.0 | 37.0 | 37.0 | 37.0 | 37.0 | 37.0 | $\begin{array}{lllllllllllll}\text { Minimum Split（s）} & 8.0 & 39.5 & 39.5 & 8.0 & 39.5 & 39.5 & 8.0 & 37.6 & 37.6 & 37.6 & 37.6 & 37.6\end{array}$ $\begin{array}{lllllllllllll}\text { Total Split（s）} & 10.0 & 45.0 & 45.0 & 27.0 & 62.0 & 62.0 & 25.0 & 88.0 & 88.0 & 63.0 & 63.0 & 63.0\end{array}$ $\begin{array}{lllllllllllll}\text { Total Split（\％）} & 6.3 \% & 28.1 \% & 28.1 \% & 16.9 \% & 38.8 \% & 38.8 \% & 15.6 \% & 55.0 \% & 55.0 \% & 39.4 \% & 39.4 \% & 39.4 \%\end{array}$ $\begin{array}{lrrrrrrrrrrrrr}\text { Maximum Green（s）} & 7.0 & 38.5 & 38.5 & 24.0 & 55.5 & 55.5 & 22.0 & 81.4 & 81.4 & 56.4 & 56.4 & 56.4 \\ \text { Yellow Time（s）} & 3.0 & 4.0 & 4.0 & 3.0 & 4.0 & 4.0 & 3.0 & 4.6 & 4.6 & 4.6 & 4.6 & 4.6\end{array}$ All－Red Time（s）


|  | 0.0 | 2.5 | 2.5 | 0.0 | 2.5 | 2.5 | 0.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| All－Red Time（s） | 0.0 | 0.0 | 0.0 | -3.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |


| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | -3.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Total Lost Time（s） | 3.0 | 6.5 | 6.5 | 0.0 | 6.5 | 6.5 | 3.0 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |


| Lead／Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead |  |  | Lag | Lag | Lag |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

 $\begin{array}{lllllllllllllll}\text { Recall Mode } & \text { None } & \text { None } & \text { None } & \text { None } & \text { None } & \text { None } & \text { None } & \text { Max } & \text { Max } & \text { Max } & \text { Max } & \text { Max }\end{array}$ Walk Time（s） $\begin{array}{rr}8.0 & 8.0 \\ 25.0 & 25.0\end{array}$

| Flash Dont Walk（s） | 25.0 | 25.0 | 25.0 | 25.0 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Pedestrian Calls（\＃hr） | 0 | 0 | 0 | 0 | 8.0 |  |  |  |  |


| Pedestrian Calls（\＃hr） |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Act Effct Green（s） | 28.1 | 17.6 | 17.6 | 51.1 | 34.6 | 34.6 | 85.1 | 81.5 | 81.5 | 64.0 | 64.0 | 64.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Actuated g／C Ratio | 0.20 | 0.13 | 0.13 | 0.37 | 0.25 | 0.25 | 0.61 | 0.59 | 0.59 | 0.46 | 0.46 | 0.46 |


| Actuated g／C Ratio | 0.20 | 0.13 | 0.13 | 0.37 | 0.25 | 0.25 | 0.61 | 0.59 | 0.59 | 0.46 | 0.46 | 0.46 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| v／c Ratio | 0.46 | 0.59 | 0.45 | 0.92 | 0.66 | 0.04 | 0.55 | 0.41 | 0.17 | 0.01 | 0.79 | 0.14 |


| Control Delay | 42.4 | 69.4 | 16.1 | 62.9 | 54.7 | 0.2 | 27.8 | 16.9 | 2.5 | 25.5 | 37.6 | 5.2 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 42.4 | 69.4 | 16.1 | 62.9 | 54.7 | 0.2 | 27.8 | 16.9 | 2.5 | 25.5 | 37.6 | 5.2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LOS | D | E | B | E | D | A | C | B | A | C | D | A |

Intersection Summary $\quad$ Other
Area Type：
Cycle Length： 160
Actuated Cycle Length： 139.2
Natural Cycle： 95
Control Type：Actuated－Uncoordinated
Maximum v／c Ratio： 0.92
Intersection Signal Delay： 35.5 Intersection LOS：D
Intersection Capacity Utilization 96．1\％
ICU Level of Service F
Analysis Period（min） 15


Queues
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Base Year: AM Peak Hour

Intersection Summary
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis


Synchro 10 Report

Lanes, Volumes, Timings

| 2: Albion Vaughan Road \& Kirby Road |  |  |  |  |  |  | Base Year: AM Peak Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 | 4 | $\uparrow$ | 1 |  | $\downarrow$ |  |
| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | M |  | $\hat{\square}$ |  |  | $\uparrow$ |  |
| Traffic Volume (vph) | , | 31 | 259 | 4 | 122 | 815 |  |
| Future Volume (vph) | 8 | 31 | 259 | 4 | 122 | 815 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Lane Width (m) | 3.7 | 3.5 | 3.7 | 3.5 | 3.7 | 3.7 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Fit | 0.893 |  | 0.998 |  |  |  |  |
| Flt Protected | 0.990 |  |  |  |  | 0.994 |  |
| Satd. Flow (prot) | 1246 | 0 | 1730 | 0 | 0 | 1852 |  |
| Flt Permitted | 0.990 |  |  |  |  | 0.994 |  |
| Satd. Flow (perm) | 1246 | 0 | 1730 | 0 | 0 | 1852 |  |
| Link Speed (k/h) | 80 |  | 60 |  |  | 60 |  |
| Link Distance (m) | 414.0 |  | 186.1 |  |  | 286.8 |  |
| Travel Time (s) | 18.6 |  | 11.2 |  |  | 17.2 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Heavy Vehicles (\%) | 88\% | 23\% | 11\% | 0\% | 4\% | 3\% |  |
| Adj. Flow (vph) | 8 | 31 | 259 | 4 | 122 | 815 |  |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 39 | 0 | 263 | 0 | 0 | 937 |  |
| Enter Blocked Intersection | No | No | No | No | No | No |  |
| Lane Alignment | Left | Right | Left | Right | Left | Left |  |
| Median Width( m ) | 3.7 |  | 0.0 |  |  | 0.0 |  |
| Link Offset(m) | 0.0 |  | 0.0 |  |  | 0.0 |  |
| Crosswalk Width(m) | 4.8 |  | 4.8 |  |  | 4.8 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |
| Headway Factor | 0.99 | 1.01 | 0.99 | 1.01 | 0.99 | 0.99 |  |
| Turning Speed (k/h) | 25 | 15 |  | 15 | 25 |  |  |
| Sign Control | Stop |  | Free |  |  | Free |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Area Type: <br> Other Control Type: Unsignalized |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 76.8\% ICU Level of Service D |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |

HCM Unsignalized Intersection Capacity Analysis
2: Albion Vaughan Road \& Kirby Road
Base Year: AM Peak Hour


Lanes, Volumes, Timings

| 3: Albion Vaughan Road \& Driveway |  |  |  |  |  |  | Base Year: AM Peak Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\Rightarrow$ |  | 4 | $\uparrow$ |  | $\downarrow$ |  |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |  |
| Lane Configurations | M |  |  | $\uparrow$ | F |  |  |
| Traffic Volume (vph) | 0 | 0 | 0 | 263 | 823 | 0 |  |
| Future Volume (vph) | 0 | 0 | 0 | 263 | 823 | 0 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Lane Width (m) | 3.7 | 3.5 | 3.7 | 3.5 | 3.7 | 3.7 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Fit |  |  |  |  |  |  |  |
| Flt Protected |  |  |  |  |  |  |  |
| Satd. Flow (prot) | 1883 | 0 | 0 | 1842 | 1883 | 0 |  |
| Flt Permitted |  |  |  |  |  |  |  |
| Satd. Flow (perm) | 1883 | 0 | 0 | 1842 | 1883 | 0 |  |
| Link Speed (khh) | 50 |  |  | 60 | 60 |  |  |
| Link Distance (m) | 75.2 |  |  | 563.9 | 186.1 |  |  |
| Travel Time (s) | 5.4 |  |  | 33.8 | 11.2 |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj. Flow (vph) | 0 | 0 | 0 | 263 | 823 | 0 |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 0 | 0 | 263 | 823 | 0 |  |
| Enter Blocked Intersection | No | No | No | No | No | No |  |
| Lane Alignment | Left | Right | Left | Left | Left | Right |  |
| Median Width( m ) | 3.7 |  |  | 3.5 | 3.5 |  |  |
| Link Offset(m) | 0.0 |  |  | 0.0 | 0.0 |  |  |
| Crosswalk Width(m) | 4.8 |  |  | 4.8 | 4.8 |  |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |
| Headway Factor | 0.99 | 1.01 | 0.99 | 1.01 | 0.99 | 0.99 |  |
| Turning Speed (kh) | 25 | 15 | 25 |  |  | 15 |  |
| Sign Control | Stop |  |  | Free | Free |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Area Type: |  |  |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 46.6\%Analysis Period (min) 15 |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |

[^9]HCM Unsignalized Intersection Capacity Analysis
3: Albion Vaughan Road \& Driveway
Base Year: AM Peak Hour


Lanes, Volumes, Timings

| 1: Regi |  |  |  |  |  |  |  |  |  | Base Yea | : PM P | k Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 |  |  | $t$ | $\leftarrow$ |  |  | 4 |  |  | $\dagger$ | $\checkmark$ |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | $\uparrow$ | F | \% | $\uparrow$ | F | ${ }^{7}$ | 个4 | F | ${ }^{7}$ | $\uparrow \uparrow$ | 7 |
| Traffic Volume (vph) | 171 | 217 | 85 | 161 | 144 | 30 | 69 | 1225 | 506 | 11 | 1020 | 141 |
| Future Volume (vph) | 171 | 217 | 85 | 161 | 144 | 30 | 69 | 1225 | 506 | 11 | 1020 | 141 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 |
| Storage Length ( m ) | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 150.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  |  |
| Taper Length ( m ) | 60.0 |  |  | 40.0 |  |  | 20.0 |  |  | 0.0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Fit |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1684 | 1746 | 1183 | 1684 | 1642 | 1298 | 1182 | 3380 | 1493 | 1513 | 3411 | 1507 |
| Fit Permitted | 0.617 |  |  | 0.440 |  |  | 0.188 |  |  | 0.203 |  |  |
| Satd. Flow (perm) | 1094 | 1746 | 1183 | 780 | 1642 | 1298 | 234 | 3380 | 1493 | 323 | 3411 | 1507 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 85 |  |  | 84 |  |  | 505 |  |  | 141 |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance ( m ) |  | 289.2 |  |  | 552.1 |  |  | 378.1 |  |  | 686.1 |  |
| Travel Time (s) |  | 17.4 |  |  | 33.1 |  |  | 19.4 |  |  | 35.3 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (\%) | 6\% | 10\% | 35\% | 6\% | 17\% | 23\% | 51\% | 8\% | 7\% | 18\% | 7\% | 6\% |
| Adj. Flow (vph) | 171 | 217 | 85 | 161 | 144 | 30 | 69 | 1225 | 506 | 11 | 1020 | 141 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 171 | 217 | 85 | 161 | 144 | 30 | 69 | 1225 | 506 | 11 | 1020 | 141 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width( m ) |  | 3.5 |  |  | 3.5 |  |  | 3.5 |  |  | 3.5 |  |
| Link Offset(m) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Crosswalk Width(m) |  | 4.8 |  |  | 4.8 |  |  | 4.8 |  |  | 4.8 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  | Yes |  |
| Headway Factor | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 |
| Turning Speed (kh) | 25 |  | 15 | 25 |  | 15 | 25 |  | 15 | 25 |  | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 |  |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector ( m ) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) |  | 9.4 |  |  | 9.4 |  |  | 9.4 |  |  | 9.4 |  |
| Detector 2 Size(m) |  | 0.6 |  |  | 0.6 |  |  | 0.6 |  |  | 0.6 |  |
| Detector 2 Type |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm |

Lanes, Volumes, Timings

| 1: Regional Road 50 | $\&$ |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Switch Phase
$\begin{array}{lllllllllllll}\text { Minimum Initial (s) } & 5.0 & 12.0 & 12.0 & 5.0 & 12.0 & 12.0 & 5.0 & 20.0 & 20.0 & 20.0 & 20.0 & 20.0 \\ \text { Minimum Silt (s) } & 8.0 & 39.5 & 39.5 & 80.0 & 39.5 & 30.0 & 8.0 & 37.0 & 37.0 & 37.0 & 37.0 & 37.0\end{array}$ $\begin{array}{lllllllllllll}\text { Minimum Split (s) } & 8.0 & 39.5 & 39.5 & 8.0 & 39.5 & 39.5 & 8.0 & 37.6 & 37.6 & 37.6 & 37.6 & 37.6\end{array}$ $\begin{array}{lcccccccccccc}\text { Total Split (s) } & 10.0 & 40.0 & 40.0 & 10.0 & 40.0 & 40.0 & 25.0 & 75.0 & 75.0 & 50.0 & 50.0 & 50.0 \\ \text { Total split (\%) } & 8.0 \% & 32.0 \% & 32.0 \% & 8.0 \% & 32.0 \% & 32.0 \% & 20.0 \% & 60.0 \% & 60.0 \% & 40.0 \% & 40.0 \% & 40.0 \%\end{array}$ $\begin{array}{lrrrrrrrrrrrr}\text { Total Split (\%) } & 8.0 \% & 32.0 \% & 32.0 \% & 8.0 \% & 32.0 \% & 32.0 \% & 20.0 \% & 60.0 \% & 60.0 \% & 40.0 \% & 40.0 \% & 40.0 \% \\ \text { Maximum Green (s) } & 7.0 & 33.5 & 33.5 & 7.0 & 33.5 & 335 & 20 & 68 . & 68 . & 43.4 & 43.4 & 43 .\end{array}$ $\begin{array}{lrrrrrrrrrrrr}\text { Maximum Green (s) } & 7.0 & 33.5 & 33.5 & 7.0 & 33.5 & 33.5 & 22.0 & 68.4 & 68.4 & 43.4 & 43.4 & 43.4 \\ \text { Yellow Time (s) } & 3.0 & 4.0 & 4.0 & 3.0 & 4.0 & 4.0 & 3.0 & 4.6 & 4.6 & 4.6 & 4.6 & 4.6\end{array}$ All-Red Time (s)

| All-Red Time (s) | 0.0 | 2.5 | 2.5 | 0.0 | 2.5 | 2.5 | 0.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0. | 0.0 | 0.0 |  |  |


| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Total Lost Time (s) | 3.0 | 6.5 | 6.5 | 3.0 | 6.5 | 6.5 | 3.0 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |


| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead |  |  | Lag | Lag | Lag |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |



 $\begin{array}{lrrrrrrrrr}\text { Walk Time (s) } & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 \\ \text { Flash Dont Walk (s) } & 250 & 250 & 250 & 250 & 23.0 & 23.0 & 230 & 23.0 & 23.0\end{array}$ $\begin{array}{lrrrrrrrrr}\text { Flash Dont Walk (s) } & 25.0 & 25.0 & 25.0 & 25.0 & 23.0 & 23.0 & 23.0 & 23.0 & 23.0 \\ \text { Pedestrian Calls (\#/hr) } & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0\end{array}$ |  | 31.5 |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Act Effct Green (s) | 31.5 | 21.0 | 21.0 | 31.5 | 21.0 | 21.0 | 72.2 | 68.5 | 68.5 | 57.7 | 57.7 | 57.7 |
| Sct | 0.28 |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{lllllllllllll}\text { Actuated g/C Ratio } & 0.28 & 0.19 & 0.19 & 0.28 & 0.19 & 0.19 & 0.64 & 0.61 & 0.61 & 0.51 & 0.51 & 0.51 \\ \text { v/c Ratio } & 0.50 & 0.67 & 0.29 & 0.59 & 0.47 & 0.10 & 0.29 & 0.60 & 0.46 & 0.07 & 0.58 & 0.17\end{array}$

| Queue Delay | 36.3 | 52.9 | 10.6 | 40.3 | 45.8 | 0.6 | 12.2 | 15.8 | 2.5 | 19.9 | 22.8 | 3.7 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
|  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |


|  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Total Delay | 36.3 | 52.9 | 10.6 | 40.3 | 45.8 | 0.6 | 12.2 | 15.8 | 2.5 | 19.9 | 22.8 |  |


| LOS | D | D | B | D | D | A | A | B | B | A | B | C |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LOpproach Delay | D | 39.3 |  |  | 39.1 |  |  | 11.9 |  |  | 20.5 | A |
| Approach LOS |  | D |  |  | D |  |  |  | B |  |  |  |

## Approach LOS

| Intersection Summary |
| :--- | :--- |
| Area Type: $\quad$ Oth |

Area Type:
Actuated Cycle Length: 112.7
Natural Cycle: 95
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.67
Intersection Signal Delay: 20.4 Intersection LOS: C
Intersection Capacity Utilization 90.6\%
ICU Level of Service E
Analysis Period (min) 15


Queues
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Base Year: PM Peak Hour

|  | 4 | $\rightarrow$ |  | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 171 | 217 | 85 | 161 | 144 | 30 | 69 | 1225 | 506 | 11 | 1020 | 141 |
| v/c Ratio | 0.50 | 0.67 | 0.29 | 0.59 | 0.47 | 0.10 | 0.29 | 0.60 | 0.46 | 0.07 | 0.58 | 0.17 |
| Control Delay | 36.3 | 52.9 | 10.6 | 40.3 | 45.8 | 0.6 | 12.2 | 15.8 | 2.5 | 19.9 | 22.8 | 3.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 36.3 | 52.9 | 10.6 | 40.3 | 45.8 | 0.6 | 12.2 | 15.8 | 2.5 | 19.9 | 22.8 | 3.7 |
| Queue Length 50th (m) | 26.7 | 41.2 | 0.0 | 24.9 | 26.2 | 0.0 | 4.9 | 74.5 | 0.1 | 1.1 | 75.7 | 0.0 |
| Queue Length 95th (m) | 42.8 | 63.7 | 11.6 | 40.7 | 43.8 | 0.0 | 12.2 | 111.7 | 13.1 | 5.1 | 115.4 | 10.6 |
| Internal Link Dist ( $m$ ) |  | 265.2 |  |  | 528.1 |  |  | 354.1 |  |  | 662.1 |  |
| Turn Bay Length ( $m$ ) | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 150.0 |
| Base Capacity (vph) | 342 | 519 | 412 | 274 | 488 | 445 | 335 | 2055 | 1105 | 165 | 1745 | 840 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.50 | 0.42 | 0.21 | 0.59 | 0.30 | 0.07 | 0.21 | 0.60 | 0.46 | 0.07 | 0.58 | 0.17 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

HCM Signalized Intersection Capacity Analysis


Lanes, Volumes, Timings

| 2: Albion Vaughan Road \& Kirby Road |  |  |  |  |  |  | Base Year: PM Peak Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 | 4 | $\uparrow$ | 1 |  | $\downarrow$ |  |
| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | M |  | $\hat{\square}$ |  |  | $\uparrow$ |  |
| Traffic Volume (vph) | 18 | 62 | 810 | 6 | 33 | 310 |  |
| Future Volume (vph) | 18 | 62 | 810 | 6 | 33 | 310 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Lane Width (m) | 3.7 | 3.5 | 3.7 | 3.5 | 3.7 | 3.7 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Fit | 0.895 |  | 0.999 |  |  |  |  |
| Flt Protected | 0.989 |  |  |  |  | 0.995 |  |
| Satd. Flow (prot) | 1560 | 0 | 1861 | 0 | 0 | 1793 |  |
| Flt Permitted | 0.989 |  |  |  |  | 0.995 |  |
| Satd. Flow (perm) | 1560 | 0 | 1861 | 0 | 0 | 1793 |  |
| Link Speed (k/h) | 80 |  | 60 |  |  | 60 |  |
| Link Distance (m) | 414.0 |  | 186.1 |  |  | 286.8 |  |
| Travel Time (s) | 18.6 |  | 11.2 |  |  | 17.2 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Heavy Vehicles (\%) | 33\% | 2\% | 3\% | 17\% | 3\% | 7\% |  |
| Adj. Flow (vph) | 18 | 62 | 810 | 6 | 33 | 310 |  |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 80 | 0 | 816 | 0 | 0 | 343 |  |
| Enter Blocked Intersection | No | No | No | No | No | No |  |
| Lane Alignment | Left | Right | Left | Right | Left | Left |  |
| Median Width( m ) | 3.7 |  | 0.0 |  |  | 0.0 |  |
| Link Offset(m) | 0.0 |  | 0.0 |  |  | 0.0 |  |
| Crosswalk Width(m) | 4.8 |  | 4.8 |  |  | 4.8 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |
| Headway Factor | 0.99 | 1.01 | 0.99 | 1.01 | 0.99 | 0.99 |  |
| Turning Speed (k/h) | 25 | 15 |  | 15 | 25 |  |  |
| Sign Control | Stop |  | Free |  |  | Free |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Area Type: ${ }_{\text {Control Type: Unsignalized }}$ Other |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |

HCM Unsignalized Intersection Capacity Analysis

| 2: Albion Vaughan Road \& Kirby Road |  |  |  |  |  |  |  | Base Year: PM Peak Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\checkmark$ | 4 | $\uparrow$ | 1 | $\checkmark$ | $\downarrow$ |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |  |
| Lane Configurations | M |  | F |  |  | $\uparrow$ |  |  |
| Traffic Volume (veh/h) | 18 | 62 | 810 | 6 | 33 | 310 |  |  |
| Future Volume (Veh/h) | 18 | 62 | 810 | 6 | 33 | 310 |  |  |
| Sign Control | Stop |  | Free |  |  | Free |  |  |
| Grade | 0\% |  | 0\% |  |  | 0\% |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Hourly flow rate (vph) | 18 | 62 | 810 | 6 | 33 | 310 |  |  |
| Pedestrians |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |
| Median type |  |  | None |  |  | None |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |
| Upstream signal ( $m$ ) |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |
| vC, conficicting volume | 1189 | 813 |  |  | 816 |  |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 1189 | 813 |  |  | 816 |  |  |  |
| tC, single (s) | 6.7 | 6.2 |  |  | 4.1 |  |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |  |
| tF (s) | 3.8 | 3.3 |  |  | 2.2 |  |  |  |
| p0 queue free \% | 90 | 84 |  |  | 96 |  |  |  |
| cM capacity (veh/h) | 173 | 378 |  |  | 807 |  |  |  |
| Direction, Lane \# | WB1 | NB 1 | SB1 |  |  |  |  |  |
| Volume Total | 80 | 816 | 343 |  |  |  |  |  |
| Volume Left | 18 | 0 | 33 |  |  |  |  |  |
| Volume Right | 62 | 6 | 0 |  |  |  |  |  |
| CSH | 299 | 1700 | 807 |  |  |  |  |  |
| Volume to Capacity | 0.27 | 0.48 | 0.04 |  |  |  |  |  |
| Queue Length 95th (m) | 7.4 | 0.0 | 0.9 |  |  |  |  |  |
| Control Delay (s) | 21.4 | 0.0 | 1.4 |  |  |  |  |  |
| Lane LOS | C |  | A |  |  |  |  |  |
| Approach Delay (s) | 21.4 | 0.0 | 1.4 |  |  |  |  |  |
| Approach LOS | C |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay 1.8 |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 55.3\% |  | CU Level of | Service | B |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |

[^10]Lanes, Volumes, Timings

| 3: Albion Vaughan Road \& Driveway |  |  |  |  |  |  | Base Year: PM Peak Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\Rightarrow$ |  | 4 | $\uparrow$ |  | $\downarrow$ |  |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |  |
| Lane Configurations | M |  |  | $\uparrow$ | A |  |  |
| Traffic Volume (vph) | 0 | 0 | 0 | 816 | 328 | 0 |  |
| Future Volume (vph) | 0 | 0 | 0 | 816 | 328 | 0 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Lane Width (m) | 3.7 | 3.5 | 3.7 | 3.5 | 3.7 | 3.7 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Fit |  |  |  |  |  |  |  |
| Flt Protected |  |  |  |  |  |  |  |
| Satd. Flow (prot) | 1883 | 0 | 0 | 1842 | 1883 | 0 |  |
| Flt Permitted |  |  |  |  |  |  |  |
| Satd. Flow (perm) | 1883 | 0 | 0 | 1842 | 1883 | 0 |  |
| Link Speed (khh) | 50 |  |  | 60 | 60 |  |  |
| Link Distance (m) | 75.2 |  |  | 552.1 | 186.1 |  |  |
| Travel Time (s) | 5.4 |  |  | 33.1 | 11.2 |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj. Flow (vph) | 0 | 0 | 0 | 816 | 328 | 0 |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 0 | 0 | 816 | 328 | 0 |  |
| Enter Blocked Intersection | No | No | No | No | No | No |  |
| Lane Alignment | Left | Right | Left | Left | Left | Right |  |
| Median Width( m ) | 3.7 |  |  | 3.5 | 3.5 |  |  |
| Link Offset(m) | 0.0 |  |  | 0.0 | 0.0 |  |  |
| Crosswalk Width(m) | 4.8 |  |  | 4.8 | 4.8 |  |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |
| Headway Factor | 0.99 | 1.01 | 0.99 | 1.01 | 0.99 | 0.99 |  |
| Turning Speed (kh) | 25 | 15 | 25 |  |  | 15 |  |
| Sign Control | Stop |  |  | Free | Free |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Area Type: |  |  |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 46.3\% ${ }^{\text {Analysis Period (min) } 15}$ ICU Level of Service A |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |

[^11]HCM Unsignalized Intersection Capacity Analysis
3: Albion Vaughan Road \& Driveway
Base Year: PM Peak Hour


[^12]
## Appendix E

## Trip Distribution Calculation

Project: 12148 Albion Vaughan Road
Project \#: 200185
Task: Trip Distribution

TTS Results

| Into/Out of | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
| Caledon | In | Out | In | Out |
| North | $20 \%$ | $3 \%$ | $6 \%$ | $9 \%$ |
| East | $0 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| South | $23 \%$ | $50 \%$ | $57 \%$ | $22 \%$ |
| West | $9 \%$ | $3 \%$ | $1 \%$ | $7 \%$ |
| Total | $51 \%$ | $56 \%$ | $64 \%$ | $38 \%$ |


| Within <br> Caledon | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | In | Out | In | Out |
| North | $46 \%$ | $40 \%$ | $27 \%$ | $52 \%$ |
| East | $0 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| South | $0 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| West | $3 \%$ | $3 \%$ | $9 \%$ | $10 \%$ |
| Total | $49 \%$ | $44 \%$ | $36 \%$ | $62 \%$ |


| All TTS <br> Zones | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | In | Out | In | Out |
| North | $65 \%$ | $44 \%$ | $33 \%$ | $61 \%$ |
| East | $0 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| South | $23 \%$ | $50 \%$ | $57 \%$ | $22 \%$ |
| West | $12 \%$ | $6 \%$ | $10 \%$ | $17 \%$ |
| Total | $100 \%$ | $100 \%$ | $100 \%$ | $100 \%$ |

TMC Travel Patterns

| Direction | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | In | Out | $\ln$ | Out |
| North | $61 \%$ | $34 \%$ | $39 \%$ | $58 \%$ |
| East | $0 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| South | $29 \%$ | $52 \%$ | $48 \%$ | $32 \%$ |
| West | $10 \%$ | $14 \%$ | $13 \%$ | $10 \%$ |

TMC Travel Patterns by Route

| Distribution by Direction (from TMCs) |  | AM Peak Hour |  | PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | IN | OUT | IN | OUT |
| North | via Regional Road 50 | 59\% | 76\% | 77\% | 62\% |
| North | via Albion Vaughan Road | 41\% | 24\% | 23\% | 38\% |
| South | via Regional Road 50 | 100\% | 100\% | 100\% | 100\% |
| West | via Mayfield Road | 100\% | 100\% | 100\% | 100\% |

Estimated Site Trip Distribution

| Distribution by Direction | AM Peak Hour |  |  | PM Peak Hour |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | IN | OUT | IN | OUT |  |  |  |  |  |  |
| North | via Regional Road 50 | $38 \%$ | $34 \%$ | $25 \%$ | $38 \%$ |  |  |  |  |  |
| North | via Albion Vaughan Road | $27 \%$ | $10 \%$ | $8 \%$ | $23 \%$ |  |  |  |  |  |
| South | via Regional Road 50 | $23 \%$ | $50 \%$ | $57 \%$ | $22 \%$ |  |  |  |  |  |
| West | via Mayfield Road | $12 \%$ | $6 \%$ | $10 \%$ | $17 \%$ |  |  |  |  |  |
| Total |  |  |  |  |  |  | $\mathbf{1 0 0} \%$ | $\mathbf{1 0 0 \%}$ | $\mathbf{1 0 0} \%$ | $\mathbf{1 0 0 \%}$ |

Note: Cross-multiplication of TTS distribution (all TTS zones) and TMC travel patterns by route

## AM Inbound

Fri Nov 182022 14:34:38 GMT-0500 (Eastern Standard Time) - Run Time: 2485ms
Cross Tabulation Query Form - Trip - 2016 v1.1
Row: 2006 GTA zone of destination - gta06_dest
Column: Planning district of origin - pd_orig

Filters
(2006 GTA zone of destination - gta06_dest In 3190
and
Start time of trip - start_time In 599-900)
Trip 2016
ROW : gta06_dest
COLUMN : pd_orig

| gta06_dest p |  | total | Jurisdiction | Study Dir | ercent |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 3190 | 10 |  | 32 Toronto | South | 1.94\% |
| 3190 | 32 |  | 115 King | North | 6.97\% |
| 3190 | 33 |  | 101 Vaughan | South | 6.12\% |
| 3190 | 34 |  | 809 Caleodn | Internal | 49.00\% |
| 3190 | 35 |  | 124 Brampton | South | 7.51\% |
|  |  |  | 123 Brampton | West | 7\% |
| 3190 | 36 |  | 58 Mississauga | South | 3.51\% |
| 3190 | 38 |  | 20 Milton | South | 1.21\% |
| 3190 | 39 |  | 12 Oakville | South | 0.73\% |
| 3190 | 72 |  | 25 Guelph/Eramosa | South | 1.51\% |
|  |  |  | 24 Guelph/Eramosa | West | 1\% |
| 3190 | 80 |  | 11 Orangeville | North | 0.67\% |
| 3190 | 84 |  | 165 Tecumseth | North | 9.99\% |
| 3190 | 85 |  | 23 Adjala-Tosorontio | North | 1.39\% |
| 3190 | 140 |  | 9 Mulmur | North | 0.55\% |

1651

AM Outbound

| Fri Nov 182022 14:36:31 GMT-0500 (Eastern Standard Time) - Run Time: 2705ms |  | AM | AM | PM | PM |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In | Out | In | Out |
| Cross Tabulation Query Form - Trip - 2016 v1.1 | North | 19.56\% | 3.45\% | 6.31\% | 9.17\% |
|  | East | 0.00\% | 0.00\% | 0.00\% | 0.00\% |
| Row: 2006 GTA zone of origin - gta06_orig | South | 22.53\% | 50.45\% | 56.53\% | 22.01\% |
| Column: Planning district of destination - pd_dest | West | 8.90\% | 2.56\% | 1.07\% | 6.94\% |
|  | Total | 51.00\% | 56.46\% | 63.92\% | 38.12\% |
| Filters: | Internal | 49.00\% | 43.54\% | 36.08\% | 61.88\% |

## PM Inbound

Fri Nov 182022 14:35:11 GMT-0500 (Eastern Standard Time) - Run Time: 2535ms
Cross Tabulation Query Form - Trip - 2016 v1.1
Row: 2006 GTA zone of destination - gta06_dest
Column: Planning district of origin - pd_orig

Filters:
(2006 GTA zone of destination - gta06_dest In 3190
and
Start time of trip - start_time In 1599-1900)


2328

PM Outbound
Fri Nov 182022 14:36:02 GMT-0500 (Eastern Standard Time) - Run Time: 3130ms
Cross Tabulation Query Form - Trip - 2016 v1. 1
Row: 2006 GTA zone of origin - gta06_orig
Column: Planning district of destination - pd_dest

Filters:
(2006 GTA zone of origin - gta06_orig In 3190
and
Start time of trip - start_time In 1599-1900)
Trip 2016
ROW : gta06_orig
COLUMN : pd dis

| gta06_orig pd_dest | st total | Jurisdiction | Study Direr Percent |  |
| :---: | :---: | :---: | :---: | :---: |
| 3190 | 5 | 9 Toronto | South | 0.54\% |
| 3190 | 10 | 43 Toronto | South | 2.59\% |
| 3190 | 14 | 8 Toronto | South | 0.48\% |
| 3190 | 32 | 39 King | North | 2.35\% |
| 3190 | 33 | 114 Vaughan | South | 6.88\% |
| 3190 | 34 | 1026 Caleodn | Internal | 61.88\% |
| 3190 | 35 | 61 Brampton | South | 3.68\% |
|  |  | 62 Brampton | West | 4\% |
| 3190 | 36 | 94 Mississauga | South | 5.67\% |
| 3190 | 39 | 12 Oakville | South | 0.72\% |
| 3190 | 72 | 24 Guelph/Eramosa | South | 1.45\% |
|  |  | 25 Guelph/Eramosa | West | 2\% |
| 3190 | 84 | 85 Tecumseth | North | 5.13\% |
| 3190 | 144 | 28 Mono | North | 1.69\% |
|  |  | 28 Mono | West | 1.69\% |

1658

2006 GTA zone of origin - gta06 orig In 319
and

Trip 2016
ROW : gta06_orig
COLUMN : pd_dest

| gta06_orig pd_des | $t$ total | Jurisdiction | Study Dires Percent |  |
| :---: | :---: | :---: | :---: | :---: |
| 3190 | 1 | 96 Toronto | South | 3.90\% |
| 3190 | 3 | 63 Toronto | South | 2.56\% |
| 3190 | 4 | 60 Toronto | South | 2.44\% |
| 3190 | 8 | 101 Toronto | South | 4.10\% |
| 3190 | 9 | 57 Toronto | South | 2.32\% |
| 3190 | 10 | 107 Toronto | South | 4.35\% |
| 3190 | 13 | 46 Toronto | South | 1.87\% |
| 3190 | 28 | 22 Aurora | North | 0.89\% |
| 3190 | 29 | 10 Richmond Hill | South | 0.41\% |
| 3190 | 31 | 23 Markham | South | 0.93\% |
| 3190 | 33 | 405 Vaughan | South | 16.45\% |
| 3190 | 34 | 1072 Caleodn | Internal | 43.54\% |
| 3190 | 35 | 64 Brampton | South | 2.60\% |
|  |  | 63 Brampton | West | 2.56\% |
| 3190 | 36 | 210 Misssssauga | South | 8.53\% |
| 3190 | 80 | 20 Orangeville | North | 0.81\% |
| 3190 | 81 | 43 Barrie | North | 1.75\% |

2462

AM Inbound
Fri Nov 182022 14:40:50 GMT-0500 (Eastern Standard Time) - Run Time: 2852ms
Cross Tabulation Query Form - Trip - 2016 v1.1
Row: 2006 GTA zone of destination - gta06_dest
Column: 2006 GTA zone of origin - gta06_orig
(2006 GTA zone of destination - gta06_dest In 3190
and
Start time of trip - start_time In 599-900
and

Trip 2016
ROW : gta06_dest

| COLUMN : gta06_orig |  |  | From TTS (1 |  | 49.00\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Study |  | Weighting |
| 3190 | 3002 | 10 | North | 1.23\% | 0.60\% |
|  |  | 9 | West | 1.11\% | 0.54\% |
| 3190 | 3003 | 27 | North | 3.33\% | 1.63\% |
| 3190 | 3152 | 41 | North | 5.06\% | 2.48\% |
|  |  | 41 | West | 5.06\% | 2.48\% |
| 3190 | 3189 | 6 | North | 0.74\% | 0.36\% |
|  |  | 7 | West | 0.86\% | 0.42\% |
| 3190 | 3190 | 418 | North | 51.60\% | 25.29\% |
| 3190 | 3192 | 32 | North | 3.95\% | 1.94\% |
| 3190 | 3193 | 157 | North | 19.38\% | 9.50\% |
| 3190 | 3194 | 55 | North | 6.79\% | 3.33\% |
| 3190 | 3195 | 7 | North | 0.86\% | 0.42\% |

810

AM Outbound
Fri Nov 182022 14:42:08 GMT-0500 (Eastern Standard Time) - Run Time: 2504ms
Cross Tabulation Query Form - Trip - 2016 v1.1

Row. 2006 GTA zone of origin - gta06_orig
Column: 2006 GTA zone of destination - gta06_dest
(2006 GTA zone of origin - gta06 orig In 3190
and
Start time of trip - start_time In 599-900
and

Trip 2016
ROW : gta06_orig

| COLUMN : gta06_dest |  |  | From TTS ( |  | 43.54\% |
| :---: | :---: | :---: | :---: | :---: | :---: |
| gta06_orig gta06_dest total |  |  | Study Dire\% |  | Weighting |
| 3190 | 3002 | 10 | North | 0.93\% | 0.41\% |
|  |  | 9 | West | 0.84\% | 0.37\% |
| 3190 | 3003 | 194 | North | 18.08\% | 7.87\% |
| 3190 | 3189 | 2 | North | 0.19\% | 0.08\% |
|  |  | 2 | West | 0.19\% | 0.08\% |
| 3190 | 3190 | 418 | North | 38.96\% | 16.96\% |
| 3190 | 3191 | 67 | West | 6.24\% | 2.72\% |
| 3190 | 3192 | 69 | North | 6.43\% | 2.80\% |
| 3190 | 3193 | 260 | North | 24.23\% | 10.55\% |
| 3190 | 3194 | 42 | North | 3.91\% | 1.70\% |

1073

## PM Inbound

Fri Nov 182022 14:41:25 GMT-0500 (Eastern Standard Time) - Run Time: 2492ms
Cross Tabulation Query Form - Trip - 2016 v1.1

Row: 2006 GTA zone of destination - gta06_dest
Column: 2006 GTA zone of origin - gta06_orig

Filters:
(2006 GTA zone of destination - gta06 dest $\ln 3190$
and
Start time of trip - start time In 1599-1900
and

Trip 2016
ROW: gta06 dest
COLUMN : gta06_orig
gta06_dest gta06_orig total

| dest gta0_orig total |  |  |  | Study Dir \% |  |  | Weighting |  |  |
| ---: | :--- | :--- | :--- | ---: | ---: | :---: | :---: | :---: | :---: |
| 3190 | 3003 | 31 | North | $3.69 \%$ | $1.33 \%$ |  |  |  |  |
| 3190 | 3010 | 23 | West | $2.74 \%$ | $0.99 \%$ |  |  |  |  |
| 3190 | 3015 | 43 | West | $5.12 \%$ | $1.85 \%$ |  |  |  |  |
| 3190 | 3100 | 14 | North | $1.67 \%$ | $0.60 \%$ |  |  |  |  |
|  |  | 14 | West | $1.67 \%$ | $0.60 \%$ |  |  |  |  |
| 3190 | 3190 | 114 | North | $13.57 \%$ | $4.90 \%$ |  |  |  |  |
| 3190 | 3191 | 136 | West | $16.19 \%$ | $5.84 \%$ |  |  |  |  |
| 3190 | 3192 | 142 | North | $16.90 \%$ | $6.10 \%$ |  |  |  |  |
| 3190 | 3193 | 188 | North | $22.38 \%$ | $8.08 \%$ |  |  |  |  |
| 3190 | 3194 | 83 | North | $9.88 \%$ | $3.57 \%$ |  |  |  |  |
| 3190 | 3195 | 36 | North | $4.29 \%$ | $1.55 \%$ |  |  |  |  |
| 3190 | 3199 | 16 | North | $1.90 \%$ | $0.69 \%$ |  |  |  |  |

PM Outbound
Fri Nov 182022 14:42:24 GMT-0500 (Eastern Standard Time) - Run Time: 3014ms
Cross Tabulation Query Form - Trip - 2016 v1.1

Row: 2006 GTA zone of origin - gta06_orig Column: 2006 GTA zone of destination - gta06_dest

Filters:
(2006 GTA zone of origin - gta06 orig In 3190
and
Start time of trip - start time In 1599-1900
and
Planning district of destination - pd_dest $\ln 34$, )
Trip 2016

| ROW : gta06_orig |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| COLUMN : gta06_dest |  |  | From TTS (PD) |  | 61.88\% |
| gta06_orig gta06_dest total |  |  | Study Dire \% |  | Weighting |
| 3190 | 3003 | 42 | North | 4.09\% | 2.53\% |
| 3190 | 3010 | 23 | West | 2.24\% | 1.39\% |
| 3190 | 3015 | 77 | West | 7.50\% | 4.64\% |
| 3190 | 3151 | 8 | North | 0.78\% | 0.48\% |
|  |  | 9 | West | 0.88\% | 0.54\% |
| 3190 | 3153 | 83 | North | 8.08\% | 5.00\% |
| 3190 | 3190 | 114 | North | 11.10\% | 6.87\% |
| 3190 | 3191 | 27 | West | 2.63\% | 1.63\% |
| 3190 | 3192 | 220 | North | 21.42\% | 13.26\% |
| 3190 | 3193 | 260 | North | 25.32\% | 15.67\% |
| 3190 | 3194 | 61 | North | 5.94\% | 3.68\% |
| 3190 | 3195 | 10 | North | 0.97\% | 0.60\% |
| 3190 | 3197 | 19 | North | 1.85\% | 1.14\% |
|  |  | 20 | West | 1.95\% | 1.21\% |
| 3190 | 3198 | 8 | North | 0.78\% | 0.48\% |
|  |  | 8 | West | 0.78\% | 0.48\% |
| 3190 | 3199 | 38 | North | 3.70\% | 2.29\% |

1027

## Appendix F

## Background Traffic Operations Reports

Lanes, Volumes, Timings
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Background: AM Peak Hour

|  | $\Rightarrow$ | $\rightarrow$ | 7 | $\downarrow$ |  | 4 | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\uparrow$ | " | ${ }^{*}$ | $\uparrow$ | 「 | \% | ¢ $\uparrow$ | " | \% | ¢ $\uparrow$ | F |
| Traffic Volume (vph) | 103 | 141 | 103 | 491 | 330 | 15 | 104 | 934 | 148 | 2 | 1406 | 103 |
| Future Volume (vph) | 103 | 141 | 103 | 491 | 330 | 15 | 104 | 934 | 148 | 2 | 1406 | 103 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 |
| Storage Length ( m ) | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 150.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length (m) | 60.0 |  |  | 40.0 |  |  | 20.0 |  |  | 0.0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1580 | 1642 | 1094 | 1767 | 1762 | 1331 | 1214 | 3411 | 1426 | 1190 | 3380 | 1465 |
| Flt Permitted | 0.561 |  |  | 0.427 |  |  | 0.055 |  |  | 0.286 |  |  |
| Satd. Flow (perm) | 933 | 1642 | 1094 | 794 | 1762 | 1331 | 70 | 3411 | 1426 | 358 | 3380 | 1465 |
| Right Turn on Red |  |  | Yes |  |  | es |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 103 |  |  | 65 |  |  | 148 |  |  | 103 |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance (m) |  | 289.2 |  |  | 563.9 |  |  | 378.1 |  |  | 686.1 |  |
| Travel Time (s) |  | 17.4 |  |  | 33.8 |  |  | 19.4 |  |  | 35.3 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (\%) | 13\% | 17\% | 46\% | 1\% | 9\% | 20\% | 47\% | 7\% | 12\% | 50\% | 8\% | 9\% |
| Adj. Flow (vph) | 103 | 141 | 103 | 491 | 330 | 15 | 104 | 934 | 148 | 2 | 1406 | 103 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 103 | 141 | 103 | 491 | 330 | 15 | 104 | 934 | 148 | 2 | 1406 | 103 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) |  | 3.5 |  |  | 3.5 |  |  | 3.5 |  |  | 3.5 |  |
| Link Offset(m) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Crosswalk Width(m) |  | 4.8 |  |  | 4.8 |  |  | 4.8 |  |  | 4.8 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  | Yes |  |
| Headway Factor | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 |
| Turning Speed (k/h) | 25 |  | 15 | 25 |  | 15 | 25 |  | 15 | 25 |  | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) |  | 9.4 |  |  | 9.4 |  |  | 9.4 |  |  | 9.4 |  |
| Detector 2 Size(m) |  | 0.6 |  |  | 0.6 |  |  | 0.6 |  |  | 0.6 |  |
| Detector 2 Type |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm |

Lanes, Volumes, Timings

1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Background: AM Peak Hour |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 1 | 6 |  |  | 2 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 1 | 6 | 6 | 2 | 2 | 2 | Switch Phase

$\begin{array}{lllllllllllll}\text { Minimum Initial (s) } & 5.0 & 12.0 & 12.0 & 5.0 & 12.0 & 12.0 & 5.0 & 20.0 & 20.0 & 20.0 & 20.0 & 20.0\end{array}$

| Minimum Split (s) | 8.0 | 39.5 | 39.5 | 8.0 | 39.5 | 39.5 | 8.0 | 37.6 | 37.6 | 37.6 | 37.6 | 37.6 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
|  | 10.0 | 29.5 | 29.5 | 39.0 | 58.5 | 58.5 | 10.0 | 51.5 | 51.5 | 75.5 | 75.5 | 75.5 | $\begin{array}{llllllllllllll}\text { Total Split (s) } & 10.0 & 29.5 & 29.5 & 39.0 & 58.5 & 58.5 & 16.0 & 91.5 & 91.5 & 75.5 & 75.5 & 75.5 \\ \text { Total Sppit (\%) } & 6.3 \% & 18.4 \% & 18.4 \% & 24.4 \% & 36.0 & 36.6 \% & 10.0 \% & 57.2 \% & 572 \% & 47.2 \% & 472 \% & 47.2 \%\end{array}$

 $\begin{array}{lrrrrrrrrrrrrr}\text { Maximum Green (s) } & 7.0 & 23.0 & 23.0 & 36.0 & 52.0 & 52.0 & 13.0 & 84.9 & 84.9 & 68.9 & 68.9 & 68.9 \\ \text { Yellow Time (s) } & 3.0 & 4.0 & 4.0 & 3.0 & 4.0 & 4.0 & 3.0 & 4.6 & 4.6 & 4.6 & 4.6 & 4.6\end{array}$ $\begin{array}{lllllllllllll}\text { Yellow Time (s) } & 3.0 & 4.0 & 4.0 & 3.0 & 4.0 & 4.0 & 3.0 & 4.6 & 4.6 & 4.0 & 4.6 & 4.6 \\ \text { All-Red Time (s) } & 0.0 & 2.5 & 2.5 & 0.0 & 2.5 & 2.5 & 0.0 & 2.0 & 2.0 & 2.0 & 2.0 & 2.0\end{array}$

| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Total Lost Time (s) | 3.0 | 6.5 | 6.5 | 3.0 | 6.5 | 6.5 | 3.0 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |


|  | Lead | Lag | Lag | Lead | Lag | Lag | Lead | 6.6 | 6.6 | 6.6 | 6.6 | 6.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Lead/Lag |  |  |  |  |  | Lag | Lag | Lag |  |  |  |  |

 $\begin{array}{llllllllllllll} & \text { Recall Mode } & \text { None } & \text { None } & \text { None None None None None } & \text { Max } & \text { Max } & \text { Max } & \text { Max }\end{array}$ $\begin{array}{lrrrrrrrrr}\text { Walk Time (s) } & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0\end{array}$ $\begin{array}{lrrrrrrrrr}\text { Flash Dont Walk (s) } & 25.0 & 25.0 & 25.0 & 25.0 & 23.0 & 23.0 & 23.0 & 23.0 & 23.0 \\ \text { Pedestrian Calls (\#/hr) } & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \end{array}$ $\begin{array}{lllllllllllll} & 19.0 \\ \text { Act Effct Green (s) } & 30.0 & 19.5 & 19.5 & 61.5 & 48.0 & 48.0 & 88.6 & 85.0 & 85.0 & 69.4 & 69.4 & 69.4\end{array}$ $\begin{array}{lllllllllllll}\text { Actuated g/C Ratio } & 0.19 & 0.12 & 0.12 & 0.39 & 0.31 & 0.31 & 0.57 & 0.54 & 0.54 & 0.44 & 0.44 & 0.44 \\ \text { v/c Ratio } & 0.50 & 0.69 & 0.46 & 0.92 & 0.61 & 0.03 & 0.79 & 0.50 & 0.18 & 0.01 & 0.94 & 0.15\end{array}$

| Control Delay | 46.3 | 83.2 | 17.0 | 63.9 | 51.4 | 0.1 | 74.4 | 23.9 | 3.1 | 26.5 | 54.0 | 5.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |


|  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | . |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Total Delay | 46.3 | 83.2 | 17.0 | 63.9 | 51.4 | 0.1 | 74.4 | 23.9 | 3.1 | 26.5 | 54.0 | 5.0 |



Intersection Summary
Anersection Summary
Area Type: Other
Area Type:
Actuated Cycle Length: 156.
Natural Cycle: 115
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.94
Intersection Signal Delay: 44.7 Intersection LOS: D
Intersection Capacity Utilization 99.4\%
ICU Level of Service F
Analysis Period (min) 15

| 401 | $\nabla_{*}{ }^{\circ}$ | $\checkmark{ }_{\square 0}$ |  | $\rightarrow_{84}$ |
| :---: | :---: | :---: | :---: | :---: |
| 16 s | 75.5 s | 39 s |  | 29.5 |
| ${ }^{4} 10$ |  | $\psi_{01} 40$ |  |  |
| 91.5 s |  | 10 s | 58.5 s |  |

## Queues

1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Background: AM Peak Hour

|  | 4 | $\rightarrow$ | 7 | $\downarrow$ | $\leftarrow$ | 4 | 4 | 4 | 7 |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 103 | 141 | 103 | 491 | 330 | 15 | 104 | 934 | 148 | 2 | 1406 | 103 |
| v/c Ratio | 0.50 | 0.69 | 0.46 | 0.92 | 0.61 | 0.03 | 0.79 | 0.50 | 0.18 | 0.01 | 0.94 | 0.15 |
| Control Delay | 46.3 | 83.2 | 17.0 | 63.9 | 51.4 | 0.1 | 74.4 | 23.9 | 3.1 | 26.5 | 54.0 | 5.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 46.3 | 83.2 | 17.0 | 63.9 | 51.4 | 0.1 | 74.4 | 23.9 | 3.1 | 26.5 | 54.0 | 5.0 |
| Queue Length 50th (m) | 19.0 | 39.3 | 0.0 | 117.1 | 80.5 | 0.0 | 19.4 | 87.8 | 0.0 | 0.3 | 203.6 | 0.0 |
| Queue Length 95th (m) | 31.5 | 61.7 | 16.9 | \#152.6 | 111.1 | 0.0 | \#50.8 | 108.0 | 10.1 | 2.1 | \#255.9 | 10.5 |
| Internal Link Dist ( $m$ ) |  | 265.2 |  |  | 539.9 |  |  | 354.1 |  |  | 662.1 |  |
| Turn Bay Length ( $m$ ) | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 150.0 |
| Base Capacity (vph) | 207 | 242 | 249 | 537 | 587 | 487 | 135 | 1856 | 843 | 159 | 1502 | 708 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.50 | 0.58 | 0.41 | 0.91 | 0.56 | 0.03 | 0.77 | 0.50 | 0.18 | 0.01 | 0.94 | 0.15 |

Intersection Summary
Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis


Synchro 10 Report

| Lanes, Volumes, Timings <br> 2: Albion Vaughan Road \& Kirby Road |  |  |  |  |  |  | Future Background: AM Peak Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\checkmark$ | 4 | $\uparrow$ | $p$ |  | $\downarrow$ |  |
| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | \% |  | f |  |  | $\uparrow$ |  |
| Traffic Volume (vph) | 8 | 31 | 298 | 4 | 122 | 936 |  |
| Future Volume (vph) | 8 | 31 | 298 | 4 | 122 | 936 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Lane Width (m) | 3.7 | 3.5 | 3.7 | 3.5 | 3.7 | 3.7 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Frt | 0.893 |  | 0.998 |  |  |  |  |
| Flt Protected | 0.990 |  |  |  |  | 0.994 |  |
| Satd. Flow (prot) | 1246 | 0 | 1730 | 0 | 0 | 1852 |  |
| Flt Permitted | 0.990 |  |  |  |  | 0.994 |  |
| Satd. Flow (perm) | 1246 | 0 | 1730 | 0 | 0 | 1852 |  |
| Link Speed (k/h) | 80 |  | 60 |  |  | 60 |  |
| Link Distance (m) | 414.0 |  | 186.1 |  |  | 286.8 |  |
| Travel Time (s) | 18.6 |  | 11.2 |  |  | 17.2 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Heavy Vehicles (\%) | 88\% | 23\% | 11\% | 0\% | 4\% | 3\% |  |
| Adj. Flow (vph) | 8 | 31 | 298 | 4 | 122 | 936 |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 39 | 0 | 302 | 0 | 0 | 1058 |  |
| Enter Blocked Intersection | No | No | No | No | No | No |  |
| Lane Alignment | Left | Right | Left | Right | Left | Left |  |
| Median Width( m ) | 3.7 |  | 0.0 |  |  | 0.0 |  |
| Link Offset(m) | 0.0 |  | 0.0 |  |  | 0.0 |  |
| Crosswalk Width(m) | 4.8 |  | 4.8 |  |  | 4.8 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |
| Headway Factor | 0.99 | 1.01 | 0.99 | 1.01 | 0.99 | 0.99 |  |
| Turning Speed (k/h) | 25 | 15 |  | 15 | 25 |  |  |
| Sign Control | Stop |  | Free |  |  | Free |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Area Type: | er |  |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 85.3\% ICU Level of Service E |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |

[^13]HCM Unsignalized Intersection Capacity Analysis
2: Albion Vaughan Road \& Kirby Road
Future Background: AM Peak Hour


[^14]Lanes, Volumes, Timings

| 3: Albion Vaughan Road \& Driveway |  |  |  |  |  |  | Future Background: AM Peak Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\Rightarrow$ |  | 4 | $\uparrow$ |  | $\downarrow$ |  |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |  |
| Lane Configurations | M |  |  | $\uparrow$ | F |  |  |
| Traffic Volume (vph) | 0 | 0 | 0 | 302 | 945 | 0 |  |
| Future Volume (vph) | 0 | 0 | 0 | 302 | 945 | 0 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Lane Width (m) | 3.7 | 3.5 | 3.7 | 3.5 | 3.7 | 3.7 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Fit |  |  |  |  |  |  |  |
| Flt Protected |  |  |  |  |  |  |  |
| Satd. Flow (prot) | 1883 | 0 | 0 | 1842 | 1883 | 0 |  |
| Flt Permitted |  |  |  |  |  |  |  |
| Satd. Flow (perm) | 1883 | 0 | 0 | 1842 | 1883 | 0 |  |
| Link Speed (khh) | 50 |  |  | 60 | 60 |  |  |
| Link Distance (m) | 75.2 |  |  | 563.9 | 186.1 |  |  |
| Travel Time (s) | 5.4 |  |  | 33.8 | 11.2 |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj. Flow (vph) | 0 | 0 | 0 | 302 | 945 | 0 |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 0 | 0 | 302 | 945 | 0 |  |
| Enter Blocked Intersection | No | No | No | No | No | No |  |
| Lane Alignment | Left | Right | Left | Left | Left | Right |  |
| Median Width( m ) | 3.7 |  |  | 3.5 | 3.5 |  |  |
| Link Offset(m) | 0.0 |  |  | 0.0 | 0.0 |  |  |
| Crosswalk Width(m) | 4.8 |  |  | 4.8 | 4.8 |  |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |
| Headway Factor | 0.99 | 1.01 | 0.99 | 1.01 | 0.99 | 0.99 |  |
| Turning Speed (kh) | 25 | 15 | 25 |  |  | 15 |  |
| Sign Control | Stop |  |  | Free | Free |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Area Type: |  |  |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 53.1\% $1 \%$ ICU Level of Service AAnalysis Period (min) 15 |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |

[^15]HCM Unsignalized Intersection Capacity Analysis
3: Albion Vaughan Road \& Driveway
Future Background: AM Peak Hour


[^16]Lanes, Volumes, Timings
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Background: PM Peak Hour

|  | $\Rightarrow$ | $\rightarrow$ |  | $t$ |  |  | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | $\uparrow$ | F | ${ }^{*}$ | $\uparrow$ | F | \% | ¢ $\uparrow$ | F | ${ }_{1}$ | $\uparrow \uparrow$ | F |
| Traffic Volume (vph) | 171 | 249 | 85 | 161 | 165 | 30 | 69 | 1407 | 506 | 11 | 1172 | 141 |
| Future Volume (vph) | 171 | 249 | 85 | 161 | 165 | 30 | 69 | 1407 | 506 | 11 | 1172 | 141 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 |
| Storage Length ( $m$ ) | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 150.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length ( m ) | 60.0 |  |  | 40.0 |  |  | 20.0 |  |  | 0.0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1684 | 1746 | 1183 | 1684 | 1642 | 1298 | 1182 | 3380 | 1493 | 1513 | 3411 | 1507 |
| Flt Permitted | 0.574 |  |  | 0.389 |  |  | 0.135 |  |  | 0.144 |  |  |
| Satd. Flow (perm) | 1017 | 1746 | 1183 | 690 | 1642 | 1298 | 168 | 3380 | 1493 | 229 | 3411 | 1507 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 85 |  |  | 84 |  |  | 458 |  |  | 141 |
| Link Speed (kh) |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance ( $m$ ) |  | 289.2 |  |  | 552.1 |  |  | 378.1 |  |  | 686.1 |  |
| Travel Time (s) |  | 17.4 |  |  | 33.1 |  |  | 19.4 |  |  | 35.3 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (\%) | 6\% | 10\% | 35\% | 6\% | 17\% | 23\% | 51\% | 8\% | 7\% | 18\% | 7\% | 6\% |
| Adj. Flow (vph) | 171 | 249 | 85 | 161 | 165 | 30 | 69 | 1407 | 506 | 11 | 1172 | 141 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 171 | 249 | 85 | 161 | 165 | 30 | 69 | 1407 | 506 | 11 | 1172 | 141 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) |  | 3.5 |  |  | 3.5 |  |  | 3.5 |  |  | 3.5 |  |
| Link Offset(m) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Crosswalk Width(m) |  | 4.8 |  |  | 4.8 |  |  | 4.8 |  |  | 4.8 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  | Yes |  |
| Headway Factor | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 |
| Turning Speed (k/h) | 25 |  | 15 | 25 |  | 15 | 25 |  | 15 | 25 |  | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector ( m ) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) |  | 9.4 |  |  | 9.4 |  |  | 9.4 |  |  | 9.4 |  |
| Detector 2 Size(m) |  | 0.6 |  |  | 0.6 |  |  | 0.6 |  |  | 0.6 |  |
| Detector 2 Type |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm |

Lanes, Volumes, Timings

Switch Phase

| Minimum Initial (s) | 5.0 | 12.0 | 12.0 | 5.0 | 12.0 | 12.0 | 5.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Minimum Split s) | 8.0 | 30. | 30.0 | 8.0 | 30.0 | 30.0 | 8.0 | 37.0 | 37.0 | 37.0 | 37.0 | 37.0 | $\begin{array}{lllllllllllll}\text { Minimum Split (s) } & 8.0 & 39.5 & 39.5 & 8.0 & 39.5 & 39.5 & 8.0 & 37.6 & 37.6 & 37.6 & 37.6 & 37.6\end{array}$ $\begin{array}{lllllllllllll}\text { Total Split (s) } & 10.0 & 40.0 & 40.0 & 10.0 & 40.0 & 40.0 & 25.0 & 75.0 & 75.0 & 50.0 & 50.0 & 50.0 \\ \text { Total Split (\%) } & 8.0 \% & 32.0 \% & 32.0 \% & 8.0 \% & 32.0 \% & 320 \% & 20 \% & 60.0 & 60.0 \% & 40.0 \% & 40.0 & 40.0\end{array}$ $\begin{array}{lllllllllllll}\text { Total Split (\%) } & 8.0 \% & 32.0 \% & 32.0 \% & 8.0 \% & 32.0 \% & 32.0 \% & 20.0 \% & 60.0 \% & 60.0 \% & 40.0 \% & 40.0 \% & 40.0 \%\end{array}$ $\begin{array}{lrrrrrrrrrrrr}\text { Maximum Green (s) } & 7.0 & 33.5 & 33.5 & 7.0 & 33.5 & 33.5 & 22.0 & 68.4 & 68.4 & 43.4 & 43.4 & 43.4 \\ \text { Yellow Time (s) } & 3.0 & 4.0 & 4.0 & 3.0 & 4.0 & 4.0 & 3.0 & 4.6 & 4.6 & 4.6 & 4.6 & 4.6\end{array}$ All-Red Time (s)


| All-Red Time (s) | 0.0 | 2.5 | 2.5 | 0.0 | 2.5 | 2.5 | 0.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Lost Time Adjust $(\mathrm{s})$ | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0. | 0. | 0.0 |  |  |


| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Total Lost Time (s) | 3.0 | 6.5 | 6.5 | 3.0 | 6.5 | 6.5 | 3.0 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |


| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead |  |  |  | Lag | Lag |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |$\quad$ Lag

 Recall Mode None None None None None None None Max Max Max Max Max $\begin{array}{lrrrrrrrrr}\text { Walk Time (s) } & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 \\ \text { Flash Dont Walk (s) } & 25.0 & 25.0 & 25.0 & 25.0 & 23.0 & 23.0 & 23.0 & 23.0 & 23.0\end{array}$ $\begin{array}{lllllllll}\text { Pedestrian Calls (\#/hr) } & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0\end{array}$ $\begin{array}{lllllllllllll}\text { Act Effict Green (s) } & 33.9 & 23.3 & 23.3 & 33.9 & 23.3 & 23.3 & 72.2 & 68.6 & 68.6 & 57.4 & 57.4 & 57.4 \\ \text { Actuated g/C Ratio } & 0.29 & 0.20 & 0.20 & 0.29 & 0.20 & 0.20 & 0.63 & 0.60 & 0.60 & 0.50 & 0.50 & 0.50\end{array}$ $\begin{array}{lllllllllllll}\text { Actuated g/C Ratio } & 0.29 & 0.20 & 0.20 & 0.29 & 0.20 & 0.20 & 0.63 & 0.60 & 0.60 & 0.50 & 0.50 & 0.50 \\ \text { v/c Ratio } & 0.50 & 0.71 & 0.28 & 0.61 & 0.50 & 0.09 & 0.35 & 0.70 & 0.47 & 0.10 & 0.69 & 0.17\end{array}$

| Control Delay | 35.8 | 53.7 | 10.0 | 41.0 | 45.6 | 0.5 | 14.8 | 19.4 | 3.5 | 23.5 | 27.1 | 4.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


|  | 35.8 | 53.7 | 10.0 | 41.0 | 45.6 | 0.5 | 14.8 | 19.4 | 3.5 | 23.5 | 27.1 | 4.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LOS | D | D | B | D | D | A | B | B | A | C | C | A |

Intersection Summary

## $\frac{\text { Intersection }}{}$

Area Type:
Cycle Length: 125
Actuated Cycle Length: 115.
Natural Cycle: 95
Control Type: Actuated-Uncoordinated $\quad$ _-
Maximum v/c Ratio: 0.71
Intersection Signal Delay: 23.3 Intersection LOS: C
Intersection Capacity Utilization 93.6\%
ICU Level of Service F
Analysis Period (min) 15


## Queues

1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Background: PM Peak Hour

|  | $\Rightarrow$ | $\rightarrow$ | 7 | 7 | $\leftarrow$ | 4 | 4 | $\dagger$ | $>$ | , | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 171 | 249 | 85 | 161 | 165 | 30 | 69 | 1407 | 506 | 11 | 1172 | 141 |
| V/c Ratio | 0.50 | 0.71 | 0.28 | 0.61 | 0.50 | 0.09 | 0.35 | 0.70 | 0.47 | 0.10 | 0.69 | 0.17 |
| Control Delay | 35.8 | 53.7 | 10.0 | 41.0 | 45.6 | 0.5 | 14.8 | 19.4 | 3.5 | 23.5 | 27.1 | 4.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 35.8 | 53.7 | 10.0 | 41.0 | 45.6 | 0.5 | 14.8 | 19.4 | 3.5 | 23.5 | 27.1 | 4.0 |
| Queue Length 50th (m) | 26.7 | 48.3 | 0.0 | 24.9 | 30.5 | 0.0 | 5.2 | 99.1 | 3.9 | 1.2 | 97.4 | 0.0 |
| Queue Length 95th (m) | 42.7 | 72.8 | 11.4 | 40.4 | 49.3 | 0.0 | 13.0 | 148.7 | 20.6 | 5.6 | 150.5 | 11.1 |
| Internal Link Dist (m) |  | 265.2 |  |  | 528.1 |  |  | 354.1 |  |  | 662.1 |  |
| Turn Bay Length (m) | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 150.0 |
| Base Capacity (vph) | 339 | 509 | 405 | 263 | 479 | 438 | 299 | 2014 | 1074 | 114 | 1700 | 822 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.50 | 0.49 | 0.21 | 0.61 | 0.34 | 0.07 | 0.23 | 0.70 | 0.47 | 0.10 | 0.69 | 0.17 |

Intersection Summary

HCM Signalized Intersection Capacity Analysis


| Lanes, Volumes, Timings <br> 2: Albion Vaughan Road \& Kirby Road |  |  |  |  |  |  | Future Background: PM Peak Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\checkmark$ | 4 | $\uparrow$ | $p$ |  | $\downarrow$ |  |
| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | \% |  | f |  |  | $\uparrow$ |  |
| Traffic Volume (vph) | 18 | 62 | 930 | 6 | 33 | 356 |  |
| Future Volume (vph) | 18 | 62 | 930 | 6 | 33 | 356 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Lane Width (m) | 3.7 | 3.5 | 3.7 | 3.5 | 3.7 | 3.7 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Frt | 0.895 |  | 0.999 |  |  |  |  |
| Flt Protected | 0.989 |  |  |  |  | 0.996 |  |
| Satd. Flow (prot) | 1560 | 0 | 1862 | 0 | 0 | 1794 |  |
| Flt Permitted | 0.989 |  |  |  |  | 0.996 |  |
| Satd. Flow (perm) | 1560 | 0 | 1862 | 0 | 0 | 1794 |  |
| Link Speed (k/h) | 80 |  | 60 |  |  | 60 |  |
| Link Distance (m) | 414.0 |  | 186.1 |  |  | 286.8 |  |
| Travel Time (s) | 18.6 |  | 11.2 |  |  | 17.2 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Heavy Vehicles (\%) | $33 \%$ | 2\% | 3\% | 17\% | 3\% | 7\% |  |
| Adj. Flow (vph) | 18 | 62 | 930 | 6 | 33 | 356 |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 80 | 0 | 936 | 0 | 0 | 389 |  |
| Enter Blocked Intersection | No | No | No | No | No | No |  |
| Lane Alignment | Left | Right | Left | Right | Left | Left |  |
| Median Width( m ) | 3.7 |  | 0.0 |  |  | 0.0 |  |
| Link Offset(m) | 0.0 |  | 0.0 |  |  | 0.0 |  |
| Crosswalk Width(m) | 4.8 |  | 4.8 |  |  | 4.8 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |
| Headway Factor | 0.99 | 1.01 | 0.99 | 1.01 | 0.99 | 0.99 |  |
| Turning Speed (k/h) | 25 | 15 |  | 15 | 25 |  |  |
| Sign Control | Stop |  | Free |  |  | Free |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Area Type: |  |  |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 60.8\% ICU Level of Service B |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |

[^17]HCM Unsignalized Intersection Capacity Analysis
2: Albion Vaughan Road \& Kirby Road
Future Background: PM Peak Hour

|  | $\dagger$ |  | $\uparrow$ | $p$ |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | M |  | $\hat{}$ |  |  | $\uparrow$ |  |
| Traffic Volume (veh/h) | 18 | 62 | 930 | 6 | 33 | 356 |  |
| Future Volume (Veh/h) | 18 | 62 | 930 | 6 | 33 | 356 |  |
| Sign Control | Stop |  | Free |  |  | Free |  |
| Grade | 0\% |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Hourly flow rate (vph) | 18 | 62 | 930 | 6 | 33 | 356 |  |
| Pedestrians |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |
| Walking Speed (m/s) |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal ( $m$ ) |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |
| vC , conflicting volume | 1355 | 933 |  |  | 936 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu , unblocked vol | 1355 | 933 |  |  | 936 |  |  |
| tC, single (s) | 6.7 | 6.2 |  |  | 4.1 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.8 | 3.3 |  |  | 2.2 |  |  |
| p0 queue free \% | 87 | 81 |  |  | 95 |  |  |
| cM capacity (veh/h) | 135 | 323 |  |  | 728 |  |  |
| Direction, Lane \# | WB 1 | NB 1 | SB 1 |  |  |  |  |
| Volume Total | 80 | 936 | 389 |  |  |  |  |
| Volume Left | 18 | 0 | 33 |  |  |  |  |
| Volume Right | 62 | 6 | 0 |  |  |  |  |
| CSH | 246 | 1700 | 728 |  |  |  |  |
| Volume to Capacity | 0.33 | 0.55 | 0.05 |  |  |  |  |
| Queue Length 95th (m) | 9.5 | 0.0 | 1.0 |  |  |  |  |
| Control Delay (s) | 26.5 | 0.0 | 1.4 |  |  |  |  |
| Lane LOS | D |  | A |  |  |  |  |
| Approach Delay (s) | 26.5 | 0.0 | 1.4 |  |  |  |  |
| Approach LOS | D |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 1.9 |  |  |  |  |
| Intersection Capacity UtilizationAnalysis Period (min) |  |  | 60.8\% | ICU Level of Service |  |  | B |
|  |  |  | 15 |  |  |  |  |

[^18]Lanes, Volumes, Timings

| 3: Albion Vaughan Road \& Driveway |  |  |  |  |  |  | Future Background: PM Peak Hour |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\Rightarrow$ |  | 4 | $\uparrow$ |  | $\downarrow$ |  |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |  |
| Lane Configurations | M |  |  | $\uparrow$ | f |  |  |
| Traffic Volume (vph) | 0 | 0 | 0 | 937 | 377 | 0 |  |
| Future Volume (vph) | 0 | 0 | 0 | 937 | 377 | 0 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Lane Width (m) | 3.7 | 3.5 | 3.7 | 3.5 | 3.7 | 3.7 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Fit |  |  |  |  |  |  |  |
| Flt Protected |  |  |  |  |  |  |  |
| Satd. Flow (prot) | 1883 | 0 | 0 | 1842 | 1883 | 0 |  |
| Flt Permitted |  |  |  |  |  |  |  |
| Satd. Flow (perm) | 1883 | 0 | 0 | 1842 | 1883 | 0 |  |
| Link Speed (khh) | 50 |  |  | 60 | 60 |  |  |
| Link Distance (m) | 75.2 |  |  | 552.1 | 186.1 |  |  |
| Travel Time (s) | 5.4 |  |  | 33.1 | 11.2 |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj. Flow (vph) | 0 | 0 | 0 | 937 | 377 | 0 |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 0 | 0 | 937 | 377 | 0 |  |
| Enter Blocked Intersection | No | No | No | No | No | No |  |
| Lane Alignment | Left | Right | Left | Left | Left | Right |  |
| Median Width( m ) | 3.7 |  |  | 3.5 | 3.5 |  |  |
| Link Offset(m) | 0.0 |  |  | 0.0 | 0.0 |  |  |
| Crosswalk Width(m) | 4.8 |  |  | 4.8 | 4.8 |  |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |
| Headway Factor | 0.99 | 1.01 | 0.99 | 1.01 | 0.99 | 0.99 |  |
| Turning Speed (kh) | 25 | 15 | 25 |  |  | 15 |  |
| Sign Control | Stop |  |  | Free | Free |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Area Type: |  |  |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 52.6\%Analysis Period (min) 15 |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |

[^19]HCM Unsignalized Intersection Capacity Analysis
3: Albion Vaughan Road \& Driveway
Future Background: PM Peak Hour

|  | $y$ |  | 4 | $\uparrow$ | $\downarrow$ | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |
| Lane Configurations | \% |  |  | $\uparrow$ | F |  |  |
| Traffic Volume (veh/h) | 0 | 0 | 0 | 937 | 377 | 0 |  |
| Future Volume (Veh/h) | 0 | 0 | 0 | 937 | 377 | 0 |  |
| Sign Control | Stop |  |  | Free | Free |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Hourly flow rate (vph) | 0 | 0 | 0 | 937 | 377 | 0 |  |
| Pedestrians |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |
| Walking Speed (m/s) |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  |  | None | None |  |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal ( $m$ ) |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |
| vC , conficting volume | 1314 | 377 | 377 |  |  |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu , unblocked vol | 1314 | 377 | 377 |  |  |  |  |
| tC, single (s) | 6.4 | 6.2 | 4.1 |  |  |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 3.3 | 2.2 |  |  |  |  |
| p0 queue free \% | 100 | 100 | 100 |  |  |  |  |
| cM capacity (veh/h) | 174 | 670 | 1181 |  |  |  |  |
| Direction, Lane \# | EB 1 | NB1 | SB 1 |  |  |  |  |
| Volume Total | 0 | 937 | 377 |  |  |  |  |
| Volume Left | 0 | 0 | 0 |  |  |  |  |
| Volume Right | 0 | 0 | 0 |  |  |  |  |
| CSH | 1700 | 1181 | 1700 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.00 | 0.22 |  |  |  |  |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Control Delay (s) | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A |  |  |  |  |  |  |
| Approach Delay (s) | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Approach LOS | A |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |
| Intersection Capacity Utilization Analysis Period (min) |  |  | 52.6\% | ICU Level of Service |  |  | A |
|  |  |  | 15 |  |  |  |  |

[^20]
## Appendix G

## Total Traffic Operations Reports

Lanes, Volumes, Timings
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Total: AM Peak Hour

|  | $\rangle$ | $\rightarrow$ |  | 7 | 4 | 4 | 4 | $\uparrow$ | + | - | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 1 | 6 |  |  | 2 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 1 | 6 | 6 | 2 | 2 | 2 |

Switch Phase
$\begin{array}{lllllllllllll}\text { Minimum Initial (s) } & 5.0 & 12.0 & 12.0 & 5.0 & 12.0 & 12.0 & 5.0 & 20.0 & 20.0 & 20.0 & 20.0 & 20.0 \\ \text { Minimum split (s) } & 8.0 & 39.5 & 39.5 & 8.0 & 3.5 & 39.5 & 8.0 & 37 . & 37 . & 37 . & 37 . & 37 .\end{array}$
$\begin{array}{lrrrrrrrrrrrr}\text { Minimum Split (s) } & 8.0 & 39.5 & 39.5 & 8.0 & 39.5 & 39.5 & 8.0 & 37.6 & 37.6 & 37.6 & 37.6 & 37.6 \\ \text { nota Split (s) } & 10.0 & 26.5 & 26.5 & 43.0 & 59.5 & 59.5 & 150 & 90.5 & 90.5 & 75.5 & 75.5 & 75.5\end{array}$
$\begin{array}{lllllllllllll} & 6.3 \% & 16.6 \% & 16.6 \% & 26.9 \% & 37.2 \% & 37.2 \% & 9.4 \% & 56.6 \% & 56.6 \% & 47.2 \% & 47.2 \% & 47.2 \%\end{array}$
$\begin{array}{lrrrrrrrrrrrrr} & 6.3 \% & 16.6 \% & 16.6 \% & 26.9 \% & 37.2 \% & 37.2 \% & 9.4 \% & 5.6 \% & 56.6 \% & 47.2 \% & 47.2 \% & 47.2 \\ \text { Maximum Green (s) } & 7.0 & 20.0 & 20.0 & 40.0 & 53.0 & 53.0 & 12.0 & 83.9 & 83.9 & 68.9 & 68.9 & 68.0\end{array}$
$\begin{array}{lrrrrrrrrrrrr}\text { Maximum Green (s) } & 7.0 & 20.0 & 20.0 & 40.0 & 53.0 & 53.0 & 12.0 & 83.9 & 83.9 & 68.9 & 68.9 & 68.9 \\ \text { Yellow Time (s) } & 3.0 & 4.0 & 4.0 & 3.0 & 4.0 & 4.0 & 3.0 & 4.6 & 4.6 & 4.6 & 4.6 & 4.6\end{array}$
$\begin{array}{lllllllllllll}\text { All-Red Time (s) } & 0.0 & 2.5 & 2.5 & 0.0 & 2.5 & 2.5 & 0.0 & 2.0 & 2.0 & 2.0 & 2.0 & 2.0\end{array}$
$\begin{array}{lllllllllllll} \\ \text { Lost Time Adjust (s) } & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0\end{array}$
$\begin{array}{llllllllllllll}\text { otal Lost Time (s) } & 3.0 & 6.5 & 6.5 & 3.0 & 6.5 & 6.5 & 3.0 & 6.6 & 6.6 & 6.6 & 6.6 & 6.6\end{array}$
Lead Lag Lag Lead Lag Lag Lead Lag Lag Lag

| ead-Lag Optimize? |  |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Vehicle Extension (s) | 5.0 | 5.0 | 5.0 |  |  |  |  |  |  |  |  |  |  |

$\begin{array}{lrrrrrrrrrrrr} & \text { None } & \text { None } & \text { None } & \text { None } & \text { None } & \text { None } & \text { None } & \text { Max } & \text { Max } & \text { Max } & \text { Max } & \text { Ma } \\ \text { Recall M Mode } & \text { No } & 8.0 & 8.0 & & 8.0 & 8.0 & & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 \\ \text { Walk Time (s) } & & 20 & & & \end{array}$
$\begin{array}{lrrrrrrrrr} & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0\end{array}$
$\begin{array}{lrrrrrrrrr}\text { Flash Dont Walk (s) } & 25.0 & 25.0 & 25.0 & 25.0 & 23.0 & 23.0 & 23.0 & 23.0 & 23.0 \\ \text { Pedestrian Calls (\#hr) } & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0\end{array}$
$\begin{array}{lllllllllllll}\text { Pedestrian Calls (\#hr) } & 29.0 & 18.5 & 18.5 & 64.8 & 51.3 & 51.3 & 87.5 & 83.9 & 83.9 & 68.9 & 68.9 & 68.9\end{array}$
$\begin{array}{lllllllllllll}\text { Act Effct Green (S) } & 0.18 & 0.12 & 0.12 & 0.41 & 0.32 & 0.32 & 0.55 & 0.53 & 0.53 & 0.44 & 0.44 & 0.44 \\ \text { Actuated g/C Ratio } & 0.52 & 0.75 \\ & 0.52 & 0.47 & \end{array}$
$\begin{array}{llllllllllllll} & 0.52 & 0.75 & 0.47 & 0.95 & 0.59 & 0.09 & 0.83 & 0.52 & 0.19 & 0.07 & 0.96 & 0.15\end{array}$
Control Delay
Control Delay
Queue Delay
otal Delay
Total Delay
Approach Delay
Approach LOS
Intersection Summary
Intersection S
Area Type:
Cycle Length: 160
Natural Cycle: 115
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.96
Itersection Signal Delay: 47.4
ntersection Capacity Utilization 101.7\%
Analysis Period (min) 15


200185-12148 Albion Vaughan Road TIS

Queues
1：Regional Road 50 \＆Mayfield Road／Albion Vaughan Road Future Total：AM Peak Hour

|  | 4 | $\rightarrow$ | v | $\checkmark$ |  | 4 | 4 | $\uparrow$ | 7 |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow（vph） | 103 | 144 | 103 | 532 | 335 | 42 | 104 | 934 | 153 | 11 | 1406 | 103 |
| V／c Ratio | 0.52 | 0.75 | 0.47 | 0.95 | 0.59 | 0.09 | 0.83 | 0.52 | 0.19 | 0.07 | 0.96 | 0.15 |
| Control Delay | 47.8 | 91.5 | 18.1 | 67.4 | 49.5 | 3.1 | 80.5 | 25.6 | 3.1 | 28.6 | 58.3 | 5.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 47.8 | 91.5 | 18.1 | 67.4 | 49.5 | 3.1 | 80.5 | 25.6 | 3.1 | 28.6 | 58.3 | 5.0 |
| Queue Length 50th（m） | 18.8 | 41.1 | 0.0 | 129.6 | 81.3 | 0.0 | 19.8 | 92.2 | 0.0 | 1.9 | 209.5 | 0.0 |
| Queue Length 95th（m） | 31.1 | \＃67．6 | 17.3 | \＃179．8 | 111.8 | 3.8 | \＃52．6 | 109.6 | 10.3 | 6.0 | \＃255．9 | 10.5 |
| Internal Link Dist（ m ） |  | 265.2 |  |  | 539.9 |  |  | 354.1 |  |  | 662.1 |  |
| Turn Bay Length（m） | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 150.0 |
| Base Capacity（vph） | 198 | 207 | 228 | 562 | 589 | 488 | 126 | 1807 | 827 | 151 | 1471 | 696 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v／c Ratio | 0.52 | 0.70 | 0.45 | 0.95 | 0.57 | 0.09 | 0.83 | 0.52 | 0.19 | 0.07 | 0.96 | 0.15 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| \＃95th percentile volume | eds ca | acity，q | ue may | be longe |  |  |  |  |  |  |  |  |

95th percentile volume exceeds capacity，queue may be longe．
Queue shown is maximum after two cycles．

HCM Signalized Intersection Capacity Analysis
1：Regional Road 50 \＆Mayfield Road／Albion Vaughan Road Future Total：AM Peak Hour

|  | $\dagger$ | $\rightarrow$ | V | $\checkmark$ |  |  | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | $\uparrow$ | 「 | \％ | $\uparrow$ | 「 | \％ | ¢ $\uparrow$ | F＇ | ${ }^{*}$ | 个个 | F |
| Traffic Volume（vph） | 103 | 144 | 103 | 532 | 335 | 42 | 104 | 934 | 153 | 11 | 1406 | 103 |
| Future Volume（vph） | 103 | 144 | 103 | 532 | 335 | 42 | 104 | 934 | 153 | 11 | 1406 | 103 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 |
| Total Lost time（s） | 3.0 | 6.5 | 6.5 | 3.0 | 6.5 | 6.5 | 3.0 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd．Flow（prot） | 1580 | 1642 | 1094 | 1767 | 1762 | 1331 | 1214 | 3411 | 1426 | 1190 | 3380 | 1465 |
| Flt Permitted | 0.56 | 1.00 | 1.00 | 0.40 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 | 0.28 | 1.00 | 1.00 |
| Satd．Flow（perm） | 929 | 1642 | 1094 | 739 | 1762 | 1331 | 71 | 3411 | 1426 | 348 | 3380 | 1465 |
| Peak－hour factor，PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj．Flow（vph） | 103 | 144 | 103 | 532 | 335 | 42 | 104 | 934 | 153 | 11 | 1406 | 103 |
| RTOR Reduction（vph） | 0 | 0 | 91 | ， | 0 | 28 | 0 | 0 | 72 | 0 | 0 | 58 |
| Lane Group Flow（vph） | 103 | 144 | 12 | 532 | 335 | 14 | 104 | 934 | 81 | 11 | 1406 | 45 |
| Heavy Vehicles（\％） | 13\％ | 17\％ | 46\％ | 1\％ | 9\％ | 20\％ | 47\％ | 7\％ | 12\％ | 50\％ | 8\％ | 9\％ |
| Turn Type | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm | Perm | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 1 | － |  |  | 2 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Actuated Green，G（s） | 25.5 | 18.5 | 18.5 | 61.3 | 51.3 | 51.3 | 83.9 | 83.9 | 83.9 | 68.9 | 68.9 | 68.9 |
| Effective Green， g （s） | 25.5 | 18.5 | 18.5 | 61.3 | 51.3 | 51.3 | 83.9 | 83.9 | 83.9 | 68.9 | 68.9 | 68.9 |
| Actuated g／C Ratio | 0.16 | 0.12 | 0.12 | 0.39 | 0.32 | 0.32 | 0.53 | 0.53 | 0.53 | 0.44 | 0.44 | 0.44 |
| Clearance Time（s） | 3.0 | 6.5 | 6.5 | 3.0 | 6.5 | 6.5 | 3.0 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |
| Vehicle Extension（s） | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Lane Grp Cap（vph） | 178 | 191 | 127 | 544 | 571 | 431 | 124 | 1807 | 755 | 151 | 1471 | 637 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | 0.03 | 0.09 |  | c0．25 | 0.19 |  | c0．06 | 0.27 |  |  | c0．42 |  |
| v／s Ratio Perm | 0.07 |  | 0.01 | c0．13 |  | 0.01 | 0.38 |  | 0.06 | 0.03 |  | 0.03 |
| v／c Ratio | 0.58 | 0.75 | 0.09 | 0.98 | 0.59 | 0.03 | 0.84 | 0.52 | 0.11 | 0.07 | 0.96 | 0.07 |
| Uniform Delay，d1 | 59.8 | 67.7 | 62.4 | 43.4 | 44.7 | 36.5 | 45.3 | 24.1 | 18.5 | 26.1 | 43.2 | 26.0 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 7.1 | 18.1 | 0.7 | 32.9 | 2.4 | 0.1 | 39.8 | 1.1 | 0.3 | 0.9 | 15.1 | 0.2 |
| Delay（s） | 66.9 | 85.8 | 63.1 | 76.3 | 47.0 | 36.6 | 85.0 | 25.1 | 18.8 | 27.0 | 58.3 | 26.3 |
| Level of Service | ， | F | ， | ， | D | D | F | C | B | C | E | C |
| Approach Delay（s） |  | 73.6 |  |  | 63.7 |  |  | 29.6 |  |  | 55.9 |  |
| Approach LOS |  | E |  |  | E |  |  | C |  |  | ， |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 51.3 |  | HCM 2000 | Level of S | Service |  | D |  |  |  |
|  |  |  | 0.97 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 158.3 |  | Sum of los | time（s） |  |  | 19.1 |  |  |  |
| Intersection Capacity Utilization |  |  | 101．7\％ |  | ICU Level | f Service |  |  | G |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

## 200185－12148 Albion Vaughan Road TIS

Synchro 10 Report

Lanes, Volumes, Timings

## 2: Albion Vaughan Road \& Kirby Road

|  | $\downarrow$ |  | $\uparrow$ | $>$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | M |  | $\hat{\beta}$ |  |  | $\uparrow$ |
| Traffic Volume (vph) | 8 | 31 | 306 | 4 | 122 | 942 |
| Future Volume (vph) | 8 | 31 | 306 | 4 | 122 | 942 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.7 | 3.5 | 3.7 | 3.5 | 3.7 | 3.7 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit | 0.893 |  | 0.998 |  |  |  |
| Flt Protected | 0.990 |  |  |  |  | 0.994 |
| Satd. Flow (prot) | 1246 | 0 | 1729 | 0 | 0 | 1852 |
| FIt Permitted | 0.990 |  |  |  |  | 0.994 |
| Satd. Flow (perm) | 1246 | 0 | 1729 | 0 | 0 | 1852 |
| Link Speed (k/h) | 80 |  | 60 |  |  | 60 |
| Link Distance (m) | 414.0 |  | 186.1 |  |  | 286.8 |
| Travel Time (s) | 18.6 |  | 11.2 |  |  | 17.2 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (\%) | 88\% | 23\% | 11\% | 0\% | 4\% | 3\% |
| Adj. Flow (vph) | 8 | 31 | 306 | 4 | 122 | 942 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Lane Group Flow (vph) | 39 | 0 | 310 | 0 | 0 | 1064 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Right | Left | Left |
| Median Width(m) | 3.7 |  | 0.0 |  |  | 0.0 |
| Link Offset(m) | 0.0 |  | 0.0 |  |  | 0.0 |
| Crosswalk Width(m) | 4.8 |  | 4.8 |  |  | 4.8 |
| Two way Left Turn Lane |  |  |  |  |  |  |
| Headway Factor | 0.99 | 1.01 | 0.99 | 1.01 | 0.99 | 0.99 |
| Turning Speed (k/h) | 25 | 15 |  | 15 | 25 |  |
| Sign Control | Stop |  | Free |  |  | Free |
| Intersection Summary |  |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Intersection Capacity Utilization 86.0\% |  |  |  | ICULevel of Service E |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |

[^21]HCM Unsignalized Intersection Capacity Analysis
2: Albion Vaughan Road \& Kirby Road
Future Total: AM Peak Hour

|  | $\downarrow$ | 4 | 4 | $p$ |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | \% |  | $\dagger$ |  |  | $\uparrow$ |  |
| Traffic Volume (veh/h) | 8 | 31 | 306 | 4 | 122 | 942 |  |
| Future Volume (Veh/h) | 8 | 31 | 306 | 4 | 122 | 942 |  |
| Sign Control | Stop |  | Free |  |  | Free |  |
| Grade | 0\% |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Hourly flow rate (vph) | 8 | 31 | 306 | 4 | 122 | 942 |  |
| Pedestrians |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |
| Walking Speed (m/s) |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal ( m ) |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |
| vC , conflicting volume | 1494 | 308 |  |  | 310 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu , unblocked vol | 1494 | 308 |  |  | 310 |  |  |
| tC, single (s) | 7.3 | 6.4 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |
| tF (s) | 4.3 | 3.5 |  |  | 2.2 |  |  |
| p0 queue free \% | 90 | 95 |  |  | 90 |  |  |
| cM capacity (veh/h) | 79 | 685 |  |  | 1239 |  |  |
| Direction, Lane \# | WB 1 | NB 1 | SB 1 |  |  |  |  |
| Volume Total | 39 | 310 | 1064 |  |  |  |  |
| Volume Left | 8 | 0 | 122 |  |  |  |  |
| Volume Right | 31 | 4 | 0 |  |  |  |  |
| cSH | 266 | 1700 | 1239 |  |  |  |  |
| Volume to Capacity | 0.15 | 0.18 | 0.10 |  |  |  |  |
| Queue Length 95th (m) | 3.5 | 0.0 | 2.3 |  |  |  |  |
| Control Delay (s) | 20.8 | 0.0 | 2.6 |  |  |  |  |
| Lane LOS | C |  | A |  |  |  |  |
| Approach Delay (s) | 20.8 | 0.0 | 2.6 |  |  |  |  |
| Approach LOS | c |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.5 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 86.0\% | ICU Level of Service |  |  | E |
| Analysis Period (min) |  |  | 15 |  |  |  |  |

200185-12148 Albion Vaughan Road TIS
Synchro 10 Repor

Lanes, Volumes, Timings
3: Albion Vaughan Road \& Driveway


[^22]HCM Unsignalized Intersection Capacity Analysis
3: Albion Vaughan Road \& Driveway


## 200185-12148 Albion Vaughan Road TIS

Synchro 10 Repor

Lanes, Volumes, Timings
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Total: PM Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{*}$ | $\uparrow$ | 「 | * | $\uparrow$ | 「 | \% | $\uparrow \uparrow$ | F | \% | $\uparrow \uparrow$ | * |
| Traffic Volume (vph) | 171 | 256 | 85 | 170 | 172 | 46 | 69 | 1407 | 541 | 27 | 1172 | 141 |
| Future Volume (vph) | 171 | 256 | 85 | 170 | 172 | 46 | 69 | 1407 | 541 | 27 | 1172 | 141 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 |
| Storage Length ( $m$ ) | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 150.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  |  |
| Taper Length (m) | 60.0 |  |  | 40.0 |  |  | 20.0 |  |  | 0.0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1684 | 1746 | 1183 | 1684 | 1642 | 1298 | 1182 | 3380 | 1493 | 1513 | 3411 | 1507 |
| Flt Permitted | 0.560 |  |  | 0.379 |  |  | 0.133 |  |  | 0.143 |  |  |
| Satd. Flow (perm) | 993 | 1746 | 1183 | 672 | 1642 | 1298 | 165 | 3380 | 1493 | 228 | 3411 | 1507 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 85 |  |  | 84 |  |  | 449 |  |  | 141 |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance ( $m$ ) |  | 289.2 |  |  | 552.1 |  |  | 378.1 |  |  | 686.1 |  |
| Travel Time (s) |  | 17.4 |  |  | 33.1 |  |  | 19.4 |  |  | 35.3 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (\%) | 6\% | 10\% | 35\% | 6\% | 17\% | 23\% | 51\% | 8\% | 7\% | 18\% | 7\% | 6\% |
| Adj. Flow (vph) | 171 | 256 | 85 | 170 | 172 | 46 | 69 | 1407 | 541 | 27 | 1172 | 141 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 171 | 256 | 85 | 170 | 172 | 46 | 69 | 1407 | 541 | 27 | 1172 | 141 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | 0 | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) |  | 3.5 |  |  | 3.5 |  |  | 3.5 |  |  | 3.5 |  |
| Link Offset(m) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Crosswalk Width(m) |  | 4.8 |  |  | 4.8 |  |  | 4.8 |  |  | 4.8 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  | Yes |  |
| Headway Factor | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 |
| Turning Speed (k/h) | 25 |  | 15 | 25 |  | 15 | 25 |  | 15 | 25 |  | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 |  |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector ( m ) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector ( m ) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) |  | 9.4 |  |  | 9.4 |  |  | 9.4 |  |  | 9.4 |  |
| Detector 2 Size(m) |  | 0.6 |  |  | 0.6 |  |  | 0.6 |  |  | 0.6 |  |
| Detector 2 Type |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm |
| 200185-12148 Albion Vaughan Road TISPTSL |  |  |  |  |  |  |  |  |  |  |  |  |

Lanes, Volumes, Timings
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Total: PM Peak Hour

|  | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Lane Group | 7 | 4 |  | 3 | 8 |  | 1 | 6 |  |  | 2 | 2 |
| Protected Phases | 4 |  | 4 | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Permitted Phases | 7 | 4 | 4 | 3 | 8 | 8 | 1 | 6 | 6 | 2 | 2 | 2 |
| Detector Phase | 7 |  |  |  |  |  |  |  |  |  |  |  |



| Minimum Initial (s) | 5.0 | 12.0 | 12.0 | 5.0 | 12.0 | 12.0 | 5.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Minimum Split (s) | 8.0 | 39.5 | 39.5 | 8.0 | 39.5 | 39.5 | 8.0 | 37.6 | 37.6 | 37.6 | 37.6 | 37.6 |


| Minimum Spit (s) | 8.0 | 39.5 | 39.5 | 8.0 | 39.5 | 39.5 | 8.0 | 37.6 | 37.6 | 37.6 | 37.6 | 37.6 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Total Split (s) | 10.0 | 40.0 | 40.0 | 10.0 | 40.0 | 40.0 | 25.0 | 75.0 | 75.0 | 50.0 | 50.0 | 50.0 |


|  | $8.0 \%$ | $32.0 \%$ | $32.0 \%$ | $8.0 \%$ | $32.0 \%$ | $32.0 \%$ | $20.0 \%$ | $60.0 \%$ | $60.0 \%$ | $40.0 \%$ | $40.0 \%$ | $40.0 \%$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | $8.0 \%$ | $32.0 \%$ | $32.0 \%$ | $8.0 \%$ | $32.0 \%$ | $32.0 \%$ | $2.0 \%$ | $60.0 \%$ | $60.0 \%$ | $40.0 \%$ | $40.0 \%$ | 40.04 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Maximum Green (s) | 7.0 | 33.5 | 33.5 | 7.0 | 33.5 | 33.5 | 22.0 | 68.4 | 68.4 | 43.4 | 43.4 | 43.4 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Yellow Time (s) | 3.0 | 4.0 | 4.0 | 3.0 | 4.0 | 4.0 | 3.0 | 4.6 | 4.6 | 4.6 | 4.6 | 4.6 |


| All-Red Time (s) | 0.0 | 2.5 | 2.5 | 0.0 | 2.5 | 2.5 | 0.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Total Lost Time (s) | 3.0 | 6.5 | 6.5 | 3.0 | 6.5 | 6.5 | 3.0 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Lead Lag Lag Lead Lag Lag Lead Lag Lag Lag

| Lead-Lag Optimize? |  |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Vehicle Extension (s) | 5.0 | 5.0 |  |  |  |  |  |  |  |  |  |  |


|  | Recall Mode | None | None | None | None | None | None | None | Max | Max | Max | Max |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Walk Time (s) |  | 8.0 | 8.0 |  | 8.0 | 8.0 |  | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |


| Valk Time (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Flash Dont Walk (s) | 25.0 | 25.0 | 25.0 | 25.0 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Pedestrian Calls (\#hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |


| Pedestrian Calls (\#hr) |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Act Effct Green (s) | 34.4 | 23.8 | 23.8 | 34.4 | 23.8 | 23.8 | 72.2 | 68.6 | 68.6 | 57.4 | 57.4 |


| Actuated g/C Ratio | 04.30 | 0.21 | 0.21 | 0.30 | 0.21 | 0.21 | 0.62 | 0.59 | 0.59 | 0.50 | 0.50 | 0.50 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 0.51 |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Ratio | 0.51 | 0.71 | 0.27 | 0.65 | 0.51 | 0.14 | 0.35 | 0.70 | 0.51 | 0.24 | 0.69 | 0.17 |


| v/C Ratio | 0.51 | 0.71 | 0.27 | 0.65 | 0.51 | 0.14 | 0.35 | 0.70 | 0.51 | 0.24 | 0.69 | 0.17 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Control Delay | 35.8 | 53.9 | 9.8 | 43.3 | 45.7 | 2.2 | 15.1 | 19.7 | 4.5 | 29.1 | 27.5 | 4.1 |


| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 35.8 | 53.9 | 9.8 | 43.3 | 45.7 | 2.2 | 15.1 | 19.7 | 4.5 | 29.1 | 27.5 | 4. |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Total Delay | D | D | A | D | D | A | B | B | A | C | C | A |


| Approach Delay | 40.5 | 39.5 | 15.5 | 25.0 |
| :--- | ---: | ---: | ---: | ---: |
| pproach LOS | D | D | B | C |

## Itersection Summary

Area Type:
Cycle Length: 125
Actuated Cycle Len
Natural Cycle: 95
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.71
$\begin{array}{ll}\text { Intersection Signal Delay: 23.7 } & \text { Intersection LOS: C } \\ \text { Intersection Capacity Utilization 94.5\% } & \text { ICU Level of Service F }\end{array}$
Analysis Period (min) 15


200185-12148 Albion Vaughan Road TIS

Queues
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Total: PM Peak Hour

|  | $\downarrow$ | $\rightarrow$ | * | $\checkmark$ |  | + | 4 | $\dagger$ | P |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 171 | 256 | 85 | 170 | 172 | 46 | 69 | 1407 | 541 | 27 | 1172 | 141 |
| v/c Ratio | 0.51 | 0.71 | 0.27 | 0.65 | 0.51 | 0.14 | 0.35 | 0.70 | 0.51 | 0.24 | 0.69 | 0.17 |
| Control Delay | 35.8 | 53.9 | 9.8 | 43.3 | 45.7 | 2.2 | 15.1 | 19.7 | 4.5 | 29.1 | 27.5 | 4.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 35.8 | 53.9 | 9.8 | 43.3 | 45.7 | 2.2 | 15.1 | 19.7 | 4.5 | 29.1 | 27.5 | 4.1 |
| Queue Length 50th (m) | 26.7 | 49.9 | 0.0 | 26.5 | 32.0 | 0.0 | 5.3 | 100.4 | 7.8 | 3.2 | 98.4 | 0.0 |
| Queue Length 95th (m) | 42.5 | 74.7 | 11.3 | 42.5 | 51.2 | 1.9 | 13.1 | 150.5 | 30.2 | 12.3 | 151.8 | 11.2 |
| Internal Link Dist (m) |  | 265.2 |  |  | 528.1 |  |  | 354.1 |  |  | 662.1 |  |
| Turn Bay Length (m) | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 150.0 |
| Base Capacity (vph) | 337 | 507 | 404 | 261 | 477 | 436 | 297 | 2005 | 1068 | 113 | 1692 | 818 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | , |  |
| Reduced v/c Ratio | 0.51 | 0.50 | 0.21 | 0.65 | 0.36 | 0.11 | 0.23 | 0.70 | 0.51 | 0.24 | 0.69 | 0.1 |

Intersection Summary

HCM Signalized Intersection Capacity Analysis
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road
Future Total: PM Peak Hour

|  | $\dagger$ | $\rightarrow$ |  |  |  |  | 4 | 4 |  |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SB |
| Lane Configurations | ${ }^{*}$ | $\uparrow$ | ${ }^{7}$ | ${ }^{*}$ | $\uparrow$ | F' | \% | 个 $\uparrow$ | " | \% | ¢ $\uparrow$ |  |
| Traffic Volume (vph) | 171 | 256 | 85 | 170 | 172 | 46 | 69 | 1407 | 541 | 27 | 1172 | 141 |
| Future Volume (vph) | 171 | 256 | 85 | 170 | 172 | 46 | 69 | 1407 | 541 | 27 | 1172 | 14 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 |
| Total Lost time (s) | 3.0 | 6.5 | 6.5 | 3.0 | 6.5 | 6.5 | 3.0 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1684 | 1746 | 1183 | 1684 | 1642 | 1298 | 1182 | 3380 | 1493 | 1513 | 3411 | 1507 |
| Flt Permitted | 0.56 | 1.00 | 1.00 | 0.38 | 1.00 | 1.00 | 0.13 | 1.00 | 1.00 | 0.14 | 1.00 | 1.00 |
| Satd. Flow (perm) | 992 | 1746 | 1183 | 671 | 1642 | 1298 | 166 | 3380 | 1493 | 228 | 3411 | 1507 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 171 | 256 | 85 | 170 | 172 | 46 | 69 | 1407 | 541 | 27 | 1172 | 141 |
| RTOR Reduction (vph) | 0 | 0 | 68 | 0 | 0 | 37 | 0 | O | 181 | 0 | 0 | 71 |
| Lane Group Flow (vph) | 171 | 256 | 17 | 170 | 172 | 9 | 69 | 1407 | 360 | 27 | 1172 | 70 |
| Heavy Vehicles (\%) | 6\% | 10\% | 35\% | 6\% | 17\% | 23\% | 51\% | 8\% | 7\% | 18\% | 7\% | 6\% |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 1 | 6 |  |  | , |  |
| Permitted Phases |  |  | 4 | 8 |  | 8 | 6 |  | 6 | 2 |  |  |
| Actuated Green, G (s) | 30.8 | 23.8 | 23.8 | 30.8 | 23.8 | 23.8 | 69.2 | 69.2 | 69.2 | 57.3 | 57.3 | 57. |
| Effective Green, $\mathrm{g}(\mathrm{s})$ | 30.8 | 23.8 | 23.8 | 30.8 | 23.8 | 23.8 | 69.2 | 69.2 | 69.2 | 57.3 | 57.3 | 57. |
| Actuated g/C Ratio | 0.27 | 0.20 | 0.20 | 0.27 | 0.20 | 0.20 | 0.60 | 0.60 | 0.60 | 0.49 | 0.49 | 0.4 |
| Clearance Time (s) | 3.0 | 6.5 | 6.5 | 3.0 | 6.5 | 6.5 | 3.0 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |
| Vehicle Extension (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | 304 | 357 | 242 | 239 | 336 | 266 | 176 | 2014 | 889 | 112 | 1683 | 743 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | 0.03 | c0.15 |  | c0.04 | 0.10 |  | 0.03 | c0.42 |  |  | 0.34 |  |
| v/s Ratio Perm | 0.11 |  | 0.01 | 0.15 |  | 0.01 | 0.20 |  | 0.24 | 0.12 |  | 0.0 |
| v/c Ratio | 0.56 | 0.72 | 0.07 | 0.71 | 0.51 | 0.04 | 0.39 | 0.70 | 0.40 | 0.24 | 0.70 | 0.0 |
| Uniform Delay, d1 | 35.8 | 43.0 | 37.2 | 37.5 | 41.0 | 37.0 | 14.2 | 16.2 | 12.5 | 16.9 | 22.7 | 15. |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.9 | 8.3 | 0.3 | 11.7 | 2.6 | 0.1 | 3.0 | 2.0 | 1.4 | 5.0 | 2.4 | 0.3 |
| Delay (s) | 39.7 | 51.3 | 37.5 | 49.2 | 43.6 | 37.1 | 17.2 | 18.3 | 13.9 | 21.9 | 25.1 | 15.9 |
| Level of Service | D | D | D | D | D | D | B | B | B | C | C |  |
| Approach Delay (s) |  | 45.1 |  |  | 45.3 |  |  | 17.0 |  |  | 24.1 |  |
| Approach LOS |  | D |  |  | D |  |  | B |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 25.2 |  | HCM 2000 | Level of S | Service |  | C |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.73 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 116.1 |  | Sum of los | time (s) |  |  | 19.1 |  |  |  |
| Intersection Capacity Utilization |  |  | 94.5\% |  | CU Level | f Service |  |  | F |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

## 200185-12148 Albion Vaughan Road TIS

Synchro 10 Repor

Lanes, Volumes, Timings
2: Albion Vaughan Road \& Kirby Road

|  | $t$ |  | 4 | P |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | M |  | $\dagger$ |  |  | $\uparrow$ |
| Traffic Volume (vph) | 18 | 62 | 940 | 6 | 33 | 361 |
| Future Volume (vph) | 18 | 62 | 940 | 6 | 33 | 361 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.7 | 3.5 | 3.7 | 3.5 | 3.7 | 3.7 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 0.895 |  | 0.999 |  |  |  |
| Flt Protected | 0.989 |  |  |  |  | 0.996 |
| Satd. Flow (prot) | 1560 | 0 | 1862 | 0 | 0 | 1794 |
| Flt Permitted | 0.989 |  |  |  |  | 0.996 |
| Satd. Flow (perm) | 1560 | 0 | 1862 | 0 | 0 | 1794 |
| Link Speed (kh) | 80 |  | 60 |  |  | 60 |
| Link Distance (m) | 414.0 |  | 186.1 |  |  | 286.8 |
| Travel Time (s) | 18.6 |  | 11.2 |  |  | 17.2 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (\%) | 33\% | 2\% | 3\% | 17\% | 3\% | 7\% |
| Adj. Flow (vph) | 18 | 62 | 940 | 6 | 33 | 361 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Lane Group Flow (vph) | 80 | 0 | 946 | 0 | 0 | 394 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Right | Left | Left |
| Median Width( m ) | 3.7 |  | 0.0 |  |  | 0.0 |
| Link Offset(m) | 0.0 |  | 0.0 |  |  | 0.0 |
| Crosswalk Width(m) | 4.8 |  | 4.8 |  |  | 4.8 |
| Two way Left Turn Lane |  |  |  |  |  |  |
| Headway Factor | 0.99 | 1.01 | 0.99 | 1.01 | 0.99 | 0.99 |
| Turning Speed (k/h) | 25 | 15 |  | 15 | 25 |  |
| Sign Control | Stop |  | Free |  |  | Free |
| Intersection Summary |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |
| Control Type: Unsignalized |  |  |  |  |  |  |
| Intersection Capacity Utilization 61.3\%Analysis Period (min) 15 |  | ICU Level of Service B |  |  |  |  |
|  |  |  |  |  |  |  |

[^23]Synchro 10 Report

HCM Unsignalized Intersection Capacity Analysis
2: Albion Vaughan Road \& Kirby Road
Future Total: PM Peak Hour

|  | $\dagger$ |  | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | M |  | $\dagger$ |  |  | $\uparrow$ |  |
| Traffic Volume (veh/h) | 18 | 62 | 940 | 6 | 33 | 361 |  |
| Future Volume (Veh/h) | 18 | 62 | 940 | 6 | 33 | 361 |  |
| Sign Control | Stop |  | Free |  |  | Free |  |
| Grade | 0\% |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Hourly flow rate (vph) | 18 | 62 | 940 | 6 | 33 | 361 |  |
| Pedestrians |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |
| Walking Speed (m/s) |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal ( $m$ ) |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |
| vC , conflicting volume | 1370 | 943 |  |  | 946 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu , unblocked vol | 1370 | 943 |  |  | 946 |  |  |
| tC , single (s) | 6.7 | 6.2 |  |  | 4.1 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.8 | 3.3 |  |  | 2.2 |  |  |
| po queue free \% | 86 | 81 |  |  | 95 |  |  |
| cM capacity (veh/h) | 132 | 318 |  |  | 721 |  |  |
| Direction, Lane \# | WB 1 | NB 1 | SB 1 |  |  |  |  |
| Volume Total | 80 | 946 | 394 |  |  |  |  |
| Volume Left | 18 | 0 | 33 |  |  |  |  |
| Volume Right | 62 | 6 | 0 |  |  |  |  |
| CSH | 242 | 1700 | 721 |  |  |  |  |
| Volume to Capacity | 0.33 | 0.56 | 0.05 |  |  |  |  |
| Queue Length 95th (m) | 9.7 | 0.0 | 1.0 |  |  |  |  |
| Control Delay (s) | 27.1 | 0.0 | 1.4 |  |  |  |  |
| Lane LOS | D |  | A |  |  |  |  |
| Approach Delay (s) | 27.1 | 0.0 | 1.4 |  |  |  |  |
| Approach LOS | D |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 1.9 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 61.3\% |  | ICU Level | Service | B |
| Analysis Period (min) |  |  | 15 |  |  |  |  |

200185-12148 Albion Vaughan Road TIS
Synchro 10 Report

Lanes, Volumes, Timings
3: Albion Vaughan Road \& Driveway

ane Width ( $m$ )
$\begin{array}{lrrrrrrr} & 10.7 & 3.5 & 3.7 & 3.5 & 3.7 & 3.7 \\ \text { ane Util. Factor } & 3.00 & 3.00 & 1.00 & 1.00 & 1.00 & 1.00\end{array}$


| Flt Protected | 0.988 |  | 0.997 |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Satd. Flow (prot) | 1669 | 0 | 0 | 1837 | 1880 | 0 |
| FIt Permitted | 0.988 |  |  | 0.997 | 180 | 0 |
| Satd. Flow (perm) | 1669 | 0 | 0 | 1837 | 1880 | 0 |

$\left.\begin{array}{lrllrrr}\text { Satd. Flow (perm) } & 1669 & 0 & 0 & 1837 & 1880 & 0\end{array}\right]$
$\begin{array}{lrrl}\text { Link Distance (m) } & 75.2 & 552.1 & 186.1\end{array}$

| Travel Time (s) | 5.4 |  | 33.1 | 11.2 |
| :--- | ---: | :--- | :--- | :--- | :--- |

$\begin{array}{lrrrrrr}\text { Peak Hour Factor } & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 & 1.00 \\ \text { Adj. Flow (vph) } & 10 & 32 & 58 & 937 & 377 & 5\end{array}$
hared Lane Traffic
$\begin{array}{lllllll} & 42 & 0 & 0 & 995 & 382 & 0\end{array}$
Enter Blocked Intersection No No No No No No
ane Alignment
Median Wain(m)
Crosswalk Width
Two way Left Turn
Headway Factor
Turning Speed (k/h)
Sign Control
Signco

| 3.7 | Left | Left |
| ---: | ---: | ---: |
|  | 3.5 | 3.5 |

Area Type:
Control Type: Unsigalized
Intersection Capacity Utilization 86.0\%
ICU Level of Service E
Analysis Period (min) 15

HCM Unsignalized Intersection Capacity Analysis
3: Albion Vaughan Road \& Driveway


[^24]Synchro 10 Report

## Appendix H

Traffic Operations Reports for Proposed Westbound Dual Left-Turn Lanes

Lanes, Volumes, Timings
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Background: AM Peak Hour

|  | $\Rightarrow$ | $\rightarrow$ | 7 | $\downarrow$ |  | 4 | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\uparrow$ | " | \% ${ }^{\text {\% }}$ | $\uparrow$ | 「 | \% | ¢ $\uparrow$ | " | \% | ¢ $\uparrow$ | F |
| Traffic Volume (vph) | 103 | 141 | 103 | 491 | 330 | 15 | 104 | 934 | 148 | 2 | 1406 | 103 |
| Future Volume (vph) | 103 | 141 | 103 | 491 | 330 | 15 | 104 | 934 | 148 | 2 | 1406 | 103 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 |
| Storage Length ( m ) | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 150.0 |
| Storage Lanes | 1 |  | 1 | 2 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length (m) | 60.0 |  |  | 40.0 |  |  | 20.0 |  |  | 0.0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1580 | 1642 | 1094 | 3429 | 1762 | 1331 | 1214 | 3411 | 1426 | 1190 | 3380 | 1465 |
| Flt Permitted | 0.527 |  |  | 0.950 |  |  | 0.059 |  |  | 0.302 |  |  |
| Satd. Flow (perm) | 876 | 1642 | 1094 | 3429 | 1762 | 1331 | 75 | 3411 | 1426 | 378 | 3380 | 1465 |
| Right Turn on Red |  |  | Yes |  |  | es |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 103 |  |  | 65 |  |  | 148 |  |  | 103 |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance (m) |  | 289.2 |  |  | 563.9 |  |  | 378.1 |  |  | 686.1 |  |
| Travel Time (s) |  | 17.4 |  |  | 33.8 |  |  | 19.4 |  |  | 35.3 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (\%) | 13\% | 17\% | 46\% | 1\% | 9\% | 20\% | 47\% | 7\% | 12\% | 50\% | 8\% | 9\% |
| Adj. Flow (vph) | 103 | 141 | 103 | 491 | 330 | 15 | 104 | 934 | 148 | 2 | 1406 | 103 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 103 | 141 | 103 | 491 | 330 | 15 | 104 | 934 | 148 | 2 | 1406 | 103 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) |  | 7.0 |  |  | 7.0 |  |  | 3.5 |  |  | 3.5 |  |
| Link Offset(m) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Crosswalk Width(m) |  | 4.8 |  |  | 4.8 |  |  | 4.8 |  |  | 4.8 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  | Yes |  |
| Headway Factor | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 |
| Turning Speed (k/h) | 25 |  | 15 | 25 |  | 15 | 25 |  | 15 | 25 |  | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) |  | 9.4 |  |  | 9.4 |  |  | 9.4 |  |  | 9.4 |  |
| Detector 2 Size(m) |  | 0.6 |  |  | 0.6 |  |  | 0.6 |  |  | 0.6 |  |
| Detector 2 Type |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | pm+pt | NA | Perm | Prot | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm |

Lanes, Volumes, Timings

1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Background: AM Peak Hour | Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Protected Phases | 7 | 4 | 4 | 3 | 8 | 8 | 1 | 6 | 6 | 2 |  | 2 |
| Permitted Phases | 4 |  | 4 |  |  | 8 | 6 |  | 6 | 2 | 2 | 2 | Detector Phas

$\begin{array}{lllllllllllll}\text { Minimum Initial (s) } & 5.0 & 12.0 & 12.0 & 5.0 & 12.0 & 12.0 & 5.0 & 20.0 & 20.0 & 20.0 & 20.0 & 20.0\end{array}$

| Minimum Split (s) | 8.0 | 39.5 | 39.5 | 8.0 | 39.5 | 39.5 | 8.0 | 37.6 | 37.6 | 37.6 | 37.6 | 37.6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | $\begin{array}{lrrrrrrrrrrrr} & 11.5 & 39.5 & 39.5 & 28.5 & 56.5 & 56.5 & 16.0 & 92.0 & 92.0 & 76.0 & 76.0 & 76.0 \\ \text { Total Split (s) } & 7.2 \% & 24.7 \% & 24.7 \% & 178 \% & 35.3 \% & 353 \% & 10.0 \% & 57.5 \% & 57.5 \% & 47.5 \% & 47.5 \% & 47.55\end{array}$ $\begin{array}{lllllllllllll}\text { Total Split (\%) } & 7.2 \% & 24.7 \% & 24.7 \% & 17.8 \% & 35.3 \% & 35.3 \% & 10.0 \% & 57.5 \% & 57.5 \% & 47.5 \% & 47.5 \% & 47.5 \%\end{array}$ $\begin{array}{lrrrrrrrrrrrrr}\text { Maximum Green (s) } & 8.5 & 33.0 & 33.0 & 25.5 & 50.0 & 50.0 & 13.0 & 85.4 & 85.4 & 69.4 & 69.4 & 69.4 \\ \text { Yellow Time (s) } & 3.0 & 4.0 & 4.0 & 3.0 & 4.0 & 4.0 & 3.0 & 4.6 & 4.6 & 4.6 & 4.6 & 4.6\end{array}$ $\begin{array}{lllllllllllll} & 3.0 & 4.0 & 4.0 & 3.0 & 4.0 & 4.0 & 3.0 & 4.6 & 4.6 & 4.6 & 4.6 & 4.0 \\ \text { All-Red Time (s) } & 0.0 & 2.5 & 2.5 & 0.0 & 2.5 & 2.5 & 0.0 & 2.0 & 2.0 & 2.0 & 2.0 & 2.0\end{array}$ $\begin{array}{lllllllllllll}\text { Lost Time Adjust (s) } & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 \\ \text { Total Lost Time (s) } & 3.0 & 6.5 & 6.5 & 3.0 & 6.5 & 6.5 & 3.0 & 6.6 & 6.6 & 6.6 & 6.6 & 6.6\end{array}$ $\begin{array}{lllllllllllll}\text { Lead/Lag } & \text { Lead } & \text { Lag } & \text { Lag } & \text { Lead } & \text { Lag } & \text { Lag } & \text { Lead } & & & \text { Lag } & \text { Lag } & \text { Lag }\end{array}$ $\begin{array}{lllllllllllllll}\text { Lead_Lag } & & \text { Lead } & \text { Lag } & \text { Lag } & \text { Lead } & \text { Lag } & \text { Lag } & \text { Lead } & & & \text { Lag } & \text { Lag } & \text { Lag } \\ \text { LeadiLag Optimize? } & & & & & & & \\ \text { Vehicle Extension (s) } & 5.0 & 5.0 & 5.0 & 5.0 & 5.0 & 5.0 & 5.0 & 5.0 & 5.0 & 5.0 & 5.0 & 5.0\end{array}$ | Recall Mode | None | None | None | Max | None | None | Min | Max | Max | Max | Max |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Max |  |  |  |  |  |  |  |  |  |  |  | $\begin{array}{lrllllllll}\text { Flash Dont Walk (s) } & 25.0 & 25.0 & 25.0 & 25.0 & 23.0 & 23.0 & 23.0 & 23.0 & 23.0\end{array}$

 $\begin{array}{lllllllllllll}\text { Act Effct Green (s) } & 32.0 & 20.0 & 20.0 & 25.5 & 37.0 & 37.0 & 89.1 & 85.5 & 85.5 & 70.0 & 70.0 & 70.0 \\ \text { Actuated g/C Ratio } & 0.22 & 0.14 & 0.14 & 0.17 & 0.25 & 0.25 & 0.61 & 0.58 & 0.58 & 0.48 & 0.48 & 0.48\end{array}$ $\begin{array}{lllllllllllll}\text { Actuated g/C Ratio } & 0.22 & 0.14 & 0.14 & 0.17 & 0.25 & 0.25 & 0.61 & 0.58 & 0.58 & 0.48 & 0.48 & 0.48 \\ \text { v/c Ratio } & 0.45 & 0.63 & 0.43 & 0.83 & 0.74 & 0.04 & 0.73 & 0.47 & 0.17 & 0.01 & 0.88 & 0.14\end{array}$

|  | 41.6 | 72.8 | 15.3 | 71.6 | 61.7 | 0.2 | 60.0 | 19.3 | 2.7 | 23.5 | 42.7 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Cuentrol Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.0 |  |  |  |  |  |  |  |  |  |  |  |


| Total Delay | 41.6 | 72.8 | 15.3 | 71.6 | 61.7 | 0.2 | 60.0 | 19.3 | 2.7 | 23.5 | 42.7 | 4.6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| LOS | D | E | B | E | E | A | E | B | A | C | D | A |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Approach Delay |  | 46.5 |  |  | 66.4 |  |  | 20.8 |  |  | 40.1 |  |

## Intersection Summary

## Area Type:

ycle Length: 160
Natural Cycle: 125
Control Type: Semi Act-Uncoord
Maximum v/c Ratio: 0.88
$\begin{array}{ll}\text { Maximum v/c Ratio: } 0.88 & \\ \text { Intersection Signal Delay: } 40.5 & \text { Intersection LOS: D } \\ \text { Intersection Capacity Utilization } 86.2 \% & \text { ICU Level of Service E }\end{array}$
Analysis Period (min) 15


## Queues

1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Background: AM Peak Hour

|  | $\Rightarrow$ | $\rightarrow$ | $\bigcirc$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | 7 |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 103 | 141 | 103 | 491 | 330 | 15 | 104 | 934 | 148 | 2 | 1406 | 103 |
| v/c Ratio | 0.45 | 0.63 | 0.43 | 0.83 | 0.74 | 0.04 | 0.73 | 0.47 | 0.17 | 0.01 | 0.88 | 0.14 |
| Control Delay | 41.6 | 72.8 | 15.3 | 71.6 | 61.7 | 0.2 | 60.0 | 19.3 | 2.7 | 23.5 | 42.7 | 4.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 41.6 | 72.8 | 15.3 | 71.6 | 61.7 | 0.2 | 60.0 | 19.3 | 2.7 | 23.5 | 42.7 | 4.6 |
| Queue Length 50th (m) | 19.1 | 36.3 | 0.0 | 66.1 | 82.1 | 0.0 | 16.1 | 72.6 | 0.0 | 0.3 | 175.3 | 0.0 |
| Queue Length 95th (m) | 31.9 | 57.3 | 15.8 | \#97.0 | 114.0 | 0.0 | \#47.1 | 101.3 | 9.5 | 1.9 | \#242.4 | 10.1 |
| Internal Link Dist (m) |  | 265.2 |  |  | 539.9 |  |  | 354.1 |  |  | 662.1 |  |
| Turn Bay Length ( $m$ ) | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 150.0 |
| Base Capacity (vph) | 231 | 368 | 325 | 594 | 599 | 495 | 146 | 1981 | 890 | 179 | 1606 | 750 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.45 | 0.38 | 0.32 | 0.83 | 0.55 | 0.03 | 0.71 | 0.47 | 0.17 | 0.01 | 0.88 | 0.14 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Intersection Summary
Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis


Synchro 10 Report

Lanes, Volumes, Timings
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Background: PM Peak Hour

|  | $\Rightarrow$ |  | \% | $t$ | $\leftarrow$ | 4 | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | $\uparrow$ | " | \%* | $\uparrow$ | 「 | \% | ¢ $\uparrow$ | " | \% | ¢ $\uparrow$ | F |
| Traffic Volume (vph) | 171 | 249 | 85 | 161 | 165 | 30 | 69 | 1407 | 506 | 11 | 1172 | 141 |
| Future Volume (vph) | 171 | 249 | 85 | 161 | 165 | 30 | 69 | 1407 | 506 | 11 | 1172 | 141 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 |
| Storage Length ( m ) | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 150.0 |
| Storage Lanes | 1 |  | 1 | 2 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length (m) | 60.0 |  |  | 40.0 |  |  | 20.0 |  |  | 0.0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1684 | 1746 | 1183 | 3267 | 1642 | 1298 | 1182 | 3380 | 1493 | 1513 | 3411 | 1507 |
| Flt Permitted | 0.595 |  |  | 0.950 |  |  | 0.130 |  |  | 0.126 |  |  |
| Satd. Flow (perm) | 1055 | 1746 | 1183 | 3267 | 1642 | 1298 | 162 | 3380 | 1493 | 201 | 3411 | 1507 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 85 |  |  | 84 |  |  | 500 |  |  | 141 |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance (m) |  | 289.2 |  |  | 552.1 |  |  | 378.1 |  |  | 686.1 |  |
| Travel Time (s) |  | 17.4 |  |  | 33.1 |  |  | 19.4 |  |  | 35.3 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (\%) | 6\% | 10\% | 35\% | 6\% | 17\% | 23\% | 51\% | 8\% | 7\% | 18\% | 7\% | 6\% |
| Adj. Flow (vph) | 171 | 249 | 85 | 161 | 165 | 30 | 69 | 1407 | 506 | 11 | 1172 | 141 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 171 | 249 | 85 | 161 | 165 | 30 | 69 | 1407 | 506 | 11 | 1172 | 141 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width( m ) |  | 7.0 |  |  | 7.0 |  |  | 3.5 |  |  | 3.5 |  |
| Link Offset(m) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Crosswalk Width(m) |  | 4.8 |  |  | 4.8 |  |  | 4.8 |  |  | 4.8 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  | Yes |  |
| Headway Factor | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 |
| Turning Speed (k/h) | 25 |  | 15 | 25 |  | 15 | 25 |  | 15 | 25 |  | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) |  | 9.4 |  |  | 9.4 |  |  | 9.4 |  |  | 9.4 |  |
| Detector 2 Size(m) |  | 0.6 |  |  | 0.6 |  |  | 0.6 |  |  | 0.6 |  |
| Detector 2 Type |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | pm+pt | NA | Perm | Prot | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm |

Lanes, Volumes, Timings

1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Background: PM Peak Hour | Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Protected Phases | 7 | 4 | 4 | 3 | 8 | 8 | 1 | 6 | 6 | 2 |  | 2 |
| Permitted Phases | 4 |  | 4 |  |  | 8 | 6 |  | 6 | 2 | 2 | 2 | Detector Phas

$\begin{array}{lllllllllllll}\text { Minimum Initial (s) } & 5.0 & 12.0 & 12.0 & 5.0 & 12.0 & 12.0 & 5.0 & 20.0 & 20.0 & 20.0 & 20.0 & 20.0\end{array}$

| Minimum Split (s) | 8.0 | 39.5 | 39.5 | 8.0 | 39.5 | 39.5 | 8.0 | 37.6 | 37.6 | 37.6 | 37.6 | 37.6 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | $\begin{array}{lrrrrrrrrrrrr}\text { Total Split (s) } & 13.0 & 39.6 & 39.6 & 14.0 & 40.6 & 40.6 & 11.0 & 71.4 & 71.4 & 60.4 & 60.4 & 60.4 \\ \text { Total Split (\%) } & 10.4 \% & 31.7 \% & 317 \% & 112 \% & 325 \% & 325 \% & 8.8 \% & 57.1 \% & 57.1 \% & 483 \% & 483 \% & 48.30\end{array}$ $\begin{array}{lllllllllllll}\text { Total Split (\%) } & 10.4 \% & 31.7 \% & 31.7 \% & 11.2 \% & 32.5 \% & 32.5 \% & 8.8 \% & 57.1 \% & 57.1 \% & 48.3 \% & 48.3 \% & 48.3 \%\end{array}$ $\begin{array}{lrrrrrrrrrrrrr}\text { Maximum Green (s) } & 10.0 & 33.1 & 33.1 & 11.0 & 34.1 & 34.1 & 8.0 & 64.8 & 64.8 & 53.8 & 53.8 & 53.8 \\ \text { Yellow Time (s) } & 3.0 & 4.0 & 4.0 & 3.0 & 4.0 & 4.0 & 3.0 & 4.6 & 4.6 & 4.6 & 4.6 & 4.6\end{array}$ All-Red Time (s)


|  | 0.0 | 2.5 | 2.5 | 0.0 | 2.5 | 2.5 | 0.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| All-Red Time (s) | 0.0 |  |  |  |  |  |  |  |  |  |  |  |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |


| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Total Lost Time (s) | 3.0 | 6.5 | 6.5 | 3.0 | 6.5 | 6.5 | 3.0 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |


| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead |  |  | 6.0 | 6.6 | Lag |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Lag |  | 6.6 | Lag |  |  |  |  |  |  |  |  |  |


 $\begin{array}{llllllllll}\text { Walk Time (s) } & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0\end{array}$ $\begin{array}{lrrrrrrrrr}\text { Flash Dont Walk (s) } & 25.0 & 25.0 & 25.0 & 25.0 & 23.0 & 23.0 & 23.0 & 23.0 & 23.0 \\ \text { Pedestrian Calls (\#/hr) } & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0\end{array}$ $\begin{array}{lllllllllllll} \\ \text { Act Effct Green (s) } & 36.9 & 23.4 & 23.4 & 10.8 & 24.1 & 24.1 & 68.6 & 65.0 & 65.0 & 56.4 & 56.4 & 56.4\end{array}$ $\begin{array}{lllllllllllll}\text { Actuated g/C Ratio } & 0.32 & 0.20 & 0.20 & 0.09 & 0.21 & 0.21 & 0.59 & 0.56 & 0.56 & 0.49 & 0.49 & 0.49 \\ \text { V/c Ratio } & 0.44 & 0.70 & 0.28 & 0.53 & 0.48 & 0.09 & 0.41 & 0.74 & 0.48 & 0.11 & 0.70 & 0.17\end{array}$

| Control Delay | 30.6 | 53.8 | 10.0 | 57.8 | 44.5 | 0.5 | 19.2 | 22.8 | 3.0 | 23.8 | 27.6 | 3.9 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Total Delay | 30.6 | 53.8 | 10.0 | 57.8 | 44.5 | 0.5 | 19.2 | 22.8 | 3.0 | 23.8 | 27.6 | 3.9 |

## OS

Aproach Delay

## Intersection Summary <br> Area Type: <br> yca Type:

Actuated Cycle Length: 115
Natural Cycle: 95
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.74
Intersection Signal Delay: 25.0 Intersection LOS: C
Intersection Capacity Utilization 91.1\%
ICU Level of Service F
Analysis Period (min) 15


## Queues

1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Background: PM Peak Hour

|  | $\Rightarrow$ | $\rightarrow$ | 7 | $\downarrow$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $>$ | , | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 171 | 249 | 85 | 161 | 165 | 30 | 69 | 1407 | 506 | 11 | 1172 | 141 |
| v/c Ratio | 0.44 | 0.70 | 0.28 | 0.53 | 0.48 | 0.09 | 0.41 | 0.74 | 0.48 | 0.11 | 0.70 | 0.17 |
| Control Delay | 30.6 | 53.8 | 10.0 | 57.8 | 44.5 | 0.5 | 19.2 | 22.8 | 3.0 | 23.8 | 27.6 | 3.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 30.6 | 53.8 | 10.0 | 57.8 | 44.5 | 0.5 | 19.2 | 22.8 | 3.0 | 23.8 | 27.6 | 3.9 |
| Queue Length 50th (m) | 25.3 | 48.5 | 0.0 | 16.6 | 30.3 | 0.0 | 5.8 | 109.2 | 0.5 | 1.3 | 101.0 | 0.0 |
| Queue Length 95th (m) | 40.5 | 72.8 | 11.3 | 28.7 | 48.9 | 0.0 | 14.1 | 160.8 | 15.6 | 5.5 | 144.5 | 10.7 |
| Internal Link Dist (m) |  | 265.2 |  |  | 528.1 |  |  | 354.1 |  |  | 662.1 |  |
| Turn Bay Length (m) | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 150.0 |
| Base Capacity (vph) | 392 | 503 | 401 | 312 | 487 | 443 | 167 | 1905 | 1060 | 98 | 1667 | 808 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.44 | 0.50 | 0.21 | 0.52 | 0.34 | 0.07 | 0.41 | 0.74 | 0.48 | 0.11 | 0.70 | 0.17 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

HCM Signalized Intersection Capacity Analysis


Lanes, Volumes, Timings
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Total: AM Peak Hour

|  | $\Rightarrow$ | $\rightarrow$ |  | 7 | 4 |  | 4 | $\uparrow$ | 7 | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 1 | 6 |  |  | 2 |  |
| Permitted Phases | 4 |  | 4 |  |  | 8 | 6 |  | 6 | 2 |  |  |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 1 | 6 | 6 | 2 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |

Switch Phase
$\begin{array}{lllllllllllll}\text { Minimum Initial (s) } & 5.0 & 12.0 & 12.0 & 5.0 & 12.0 & 12.0 & 5.0 & 20.0 & 20.0 & 20.0 & 20.0 & 20.0 \\ \text { Minimum split (s) } & 8.0 & 39.5 & 39.5 & 8.0 & 39.5 & 39.5 & 8.0 & 37 . & 37.0 & 37.0 & 37.0 & 37.0\end{array}$
$\begin{array}{lrrrrrrrrrrrr}\text { Minimum Split (s) } & 8.0 & 39.5 & 39.5 & 8.0 & 39.5 & 39.5 & 8.0 & 37.6 & 37.6 & 37.6 & 37.6 & 37.6\end{array}$

| otal Split (\%) | $6.3 \%$ | $24.4 \%$ | $24.4 \%$ | $18.1 \%$ | $36.3 \%$ | $36.3 \%$ | $10.0 \%$ | $57.5 \%$ | $57.5 \%$ | $47.5 \%$ | $47.5 \%$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

$\begin{array}{lrrrrrrrrrrrr} \\ \text { Maximum Green (s) } & 6.3 \% & 24.4 \% & 24.4 \% & 18.1 \% & 36.3 \% & 36.3 \% & 10.0 \% & 57.5 \% & 57.5 \% & 47.5 \% & 47.5 \% & 47.5 \% \\ & 7.0 & 32.5 & 32.5 & 26.0 & 51.5 & 51.5 & 13.0 & 85.4 & 85.4 & 69.4 & 69.4 & 69.4\end{array}$
$\begin{array}{lrrrrrrrrrrrr}\text { Maximum Green (s) } & 7.0 & 32.5 & 32.5 & 26.0 & 51.5 & 51.5 & 13.0 & 85.4 & 85.4 & 69.4 & 69.4 & 69.4 \\ \text { Yellow Time (s) } & 3.0 & 4.0 & 4.0 & 3.0 & 4.0 & 4.0 & 3.0 & 4.6 & 4.6 & 4.6 & 4.6 & 4.6\end{array}$
$\begin{array}{lllllllllllll}\text { All-Red Time (s) } & 0.0 & 2.5 & 2.5 & 0.0 & 2.5 & 2.5 & 0.0 & 2.0 & 2.0 & 2.0 & 2.0 & 2.0\end{array}$
$\begin{array}{lllllllllllll}\text { Lost Time Adjust (s) } & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0\end{array}$
$\begin{array}{llllllllllllll}\text { otal Lost Time (s) } & 3.0 & 6.5 & 6.5 & 3.0 & 6.5 & 6.5 & 3.0 & 6.6 & 6.6 & 6.6 & 6.6 & 6.6\end{array}$
Lead/Lag Lead Lag Lead Lag Lag Lead Lag Lag Lag
$\begin{array}{lllllllllllll}\text { Lead-Lag Optimize? } & & & & & & & & \\ \text { Vehicle Extension (s) } & 5.0 & 5.0 & 5.0 & 5.0 & 5.0 & 5.0 & 5.0 & 5.0 & 5.0 & 5.0 & 5.0\end{array}$
$\begin{array}{lrrrrrrrrrrrr} & \text { None } & \text { None } & \text { None } & \text { None } & \text { None } & \text { None } & \text { None } & \text { Max } & \text { Max } & \text { Max } & \text { Max } & \text { Ma } \\ \text { Recall M Mode } & \text { No } & 8.0 & 8.0 & & 8.0 & 8.0 & & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 \\ \text { Walk Time (s) } & & 20 & & & \end{array}$
$\begin{array}{lrrrrrrrrr} & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 & 8.0 \\ \text { Walk Time (s) } & 25.0 & 25.0 & 25.0 & 25.0 & 23.0 & 23.0 & 23.0 & 23.0 & 23.0\end{array}$

| Flash Dont Walk (s) |  | 25.0 | 25.0 |  | 25.0 | 25.0 |  | 23.0 | 23.0 | 23.0 | 23.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| (s) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pedestrian Calls (\#hr) | 30.4 | 19.9 | 19.9 | 26.0 | 38.9 | 38.9 | 89.1 | 85.5 | 85.5 | 69.9 | 69.9 |
| Act Effct Green (s) | 0.29 .9 |  |  |  |  |  |  |  |  |  |  |



|  | 0.21 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


$\begin{array}{lrrrrrrrrrrrrr} & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0\end{array}$
$\begin{array}{lrrrrrrrrrrrr}\text { Queue Delay } & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 & 0.0 \\ \text { Total Delay } & 44.2 & 74.3 & 15.5 & 76.4 & 58.9 & 3.7 & 60.9 & 19.5 & 2.7 & 24.5 & 43.1 & 4.6 \\ \text { OS } & \text { D } & \text { E } & \text { B } & \text { E } & \text { E } & \text { A } & \text { E } & \text { B } & \text { A } & \text { C } & \text { D } & \text { A }\end{array}$
Approach Delay
Approach LOS
Intersection Summary
Area Type:
Cycle Length: 160
Cyctuated Cycle Length:
Natural Cycle: 135
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.88
tersection Signal Delay: 41.2
Intersection Capacity Utilization 87.4\%
Analysis Period (min) 15


200185-12148 Albion Vaughan Road TIS

Queues
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Total: AM Peak Hour

|  | $\stackrel{ }{*}$ | $\rightarrow$ | \% | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\dagger$ | 1 |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 103 | 144 | 103 | 532 | 335 | 42 | 104 | 934 | 153 | 11 | 1406 | 103 |
| v/c Ratio | 0.46 | 0.65 | 0.44 | 0.88 | 0.72 | 0.11 | 0.74 | 0.47 | 0.17 | 0.06 | 0.88 | 0.14 |
| Control Delay | 44.2 | 74.3 | 15.5 | 76.4 | 58.9 | 3.7 | 60.9 | 19.5 | 2.7 | 24.5 | 43.1 | 4.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 44.2 | 74.3 | 15.5 | 76.4 | 58.9 | 3.7 | 60.9 | 19.5 | 2.7 | 24.5 | 43.1 | 4.6 |
| Queue Length 50th (m) | 19.1 | 37.3 | 0.0 | 72.8 | 82.4 | 0.0 | 16.4 | 73.7 | 0.0 | 1.6 | 177.3 | 0.0 |
| Queue Length 95th (m) | 32.1 | 58.5 | 16.1 | \#107.5 | 114.1 | 3.8 | \#46.6 | 99.5 | 9.5 | 5.6 | \#233.0 | 10.2 |
| Internal Link Dist (m) |  | 265.2 |  |  | 539.9 |  |  | 354.1 |  |  | 662.1 |  |
| Turn Bay Length (m) | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 50.0 |
| Base Capacity (vph) | 222 | 362 | 321 | 604 | 615 | 507 | 145 | 1976 | 890 | 178 | 1602 | 748 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.46 | 0.40 | 0.32 | 0.88 | 0.54 | 0.08 | 0.72 | 0.47 | 0.17 | 0.06 | 0.88 | 0.14 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road
Future Total: AM Peak Hour


## 200185-12148 Albion Vaughan Road TIS

Synchro 10 Report

Lanes, Volumes, Timings
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Total: PM Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{*}$ | $\uparrow$ | 「 | \%* | $\uparrow$ | 7 | \% | ¢ $\uparrow$ | F' | \% | ¢ $\uparrow$ | 7 |
| Traffic Volume (vph) | 171 | 256 | 85 | 170 | 172 | 46 | 69 | 1407 | 541 | 27 | 1172 | 141 |
| Future Volume (vph) | 171 | 256 | 85 | 170 | 172 | 46 | 69 | 1407 | 541 | 27 | 1172 | 141 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 |
| Storage Length ( m ) | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 50.0 |
| Storage Lanes | 1 |  | 1 | 2 |  | 1 | 1 |  | 1 | 1 |  |  |
| Taper Length ( m ) | 60.0 |  |  | 40.0 |  |  | 20.0 |  |  | 0.0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Fit |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1684 | 1746 | 1183 | 3267 | 1642 | 1298 | 1182 | 3380 | 1493 | 1513 | 3411 | 1507 |
| Flt Permitted | 0.583 |  |  | 0.950 |  |  | 0.129 |  |  | 0.124 |  |  |
| Satd. Flow (perm) | 1033 | 1746 | 1183 | 3267 | 1642 | 1298 | 161 | 3380 | 1493 | 197 | 3411 | 1507 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Ye |  |  |  |
| Satd. Flow (RTOR) |  |  | 85 |  |  | 84 |  |  | 492 |  |  | 141 |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance (m) |  | 289.2 |  |  | 552.1 |  |  | 378.1 |  |  | 686.1 |  |
| Travel Time (s) |  | 17.4 |  |  | 33.1 |  |  | 19.4 |  |  | 35.3 |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Heavy Vehicles (\%) | 6\% | 10\% | 35\% | 6\% | 17\% | 23\% | 51\% | 8\% | 7\% | 18\% | 7\% | 6\% |
| Adj. Flow (vph) | 171 | 256 | 85 | 170 | 172 | 46 | 69 | 1407 | 541 | 27 | 1172 | 141 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 171 | 256 | 85 | 170 | 172 | 46 | 69 | 1407 | 541 | 27 | 1172 | 141 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Righ |
| Median Width(m) |  | 7.0 |  |  | 7.0 |  |  | 3.5 |  |  | 3.5 |  |
| Link Offset(m) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Crosswalk Width(m) |  | 4.8 |  |  | 4.8 |  |  | 4.8 |  |  | 4.8 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  | Yes |  |
| Headway Factor | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 | 1.01 | 0.99 | 1.01 |
| Turning Speed (k/h) | 25 |  | 15 | 25 |  | 15 | 25 |  | 15 | 25 |  | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 |  |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector ( m ) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) |  | 9.4 |  |  | 9.4 |  |  | 9.4 |  |  | 9.4 |  |
| Detector 2 Size(m) |  | 0.6 |  |  | 0.6 |  |  | 0.6 |  |  | 0.6 |  |
| Detector 2 Type |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |  | $\mathrm{Cl}+\mathrm{Ex}$ |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | pm+pt | NA | Perm | Prot | NA | Perm | pm+pt | NA | Perm | Perm | NA | Pe |

Lanes, Volumes, Timings
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Total: PM Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 1 | 6 |  |  | 2 | 2 |
| Permitted Phases | 4 |  | 4 |  |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 1 | 6 | 6 | 2 | 2 | 2 |

Detector Phase


| Minimum Initial (s) | 5.0 | 12.0 | 12.0 | 5.0 | 12.0 | 12.0 | 5.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Minimum Split (s) | 8.0 | 39.5 | 39.5 | 8.0 | 39.5 | 39.5 | 8.0 | 37.6 | 37.6 | 37.6 | 37.6 | 37.6 |


| Minimum Split (s) | 8.0 | 39.5 | 39.5 | 8.0 | 39.5 | 39.5 | 8.0 | 37.6 | 37.6 | 37.6 | 37.6 | 37.6 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Total Split (s) | 13.0 | 39.6 | 39.6 | 14.0 | 40.6 | 40.6 | 11.0 | 71.4 | 71.4 | 60.4 | 60.4 | 60.4 |


| Total Spiti (s) | $10.4 \%$ | $31.7 \%$ | $31.7 \%$ | $11.2 \%$ | $32.5 \%$ | $32.5 \%$ | $8.8 \%$ | $57.1 \%$ | $57.1 \%$ | $48.3 \%$ | $48.3 \%$ | $48.3 \%$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Total Split (\%) | $10.4 \%$ | $31.7 \%$ | $31.7 \%$ | $11.2 \%$ | $32.5 \%$ | $32.5 \%$ | $8.8 \%$ | $57.1 \%$ | $57.1 \%$ | $48.3 \%$ | $48.3 \%$ | $48.3 \%$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Maximum Green (s) | 10.0 | 33.1 | 33.1 | 11.0 | 34.1 | 34.1 | 8.0 | 64.8 | 64.8 | 53.8 | 538 | 53.8 |


| Maximum Green (s) | 10.0 | 33.1 | 33.1 | 11.0 | 34.1 | 34.1 | 8.0 | 64.8 | 64.8 | 53.8 | 53.8 | 53.8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Yellow Time (s) | 3.0 | 4.0 | 4.0 | 3.0 | 4.0 | 4.0 | 3.0 | 4.6 | 4.6 | 4.6 | 4.6 | 4.6 |


| All-Red Time (s) | 0.0 | 2.5 | 2.5 | 0.0 | 2.5 | 2.5 | 0.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Total Lost Time (s) | 3.0 | 6.5 | 6.5 | 3.0 | 6.5 | 6.5 | 3.0 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Lead Lag Lag Lead Lag Lag Lead Lag Lag Lag

| Lead-Lag Optimize? | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Vehicle Extension (s) | 5.0 |  |  |  |  |  |  |  |  |  |  |  |


|  | None | None | None | None | None | None | None | Max | Max | Max | Max |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Recall Mode | Max |  |  |  |  |  |  |  |  |  |  |
| Walk Time (s) |  | 8.0 | 8.0 |  | 8.0 | 8.0 |  | 8.0 | 8.0 | 8.0 | 8.0 |
| 8.0 |  |  |  |  |  |  |  |  |  |  |  |


| Nalk Time (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Flash Dont Walk (s) | 25.0 | 25.0 | 25.0 | 25.0 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Pedestrian Calls (\#hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |


| Pedestrian Calls (\#/hr) |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Act Efft Green (s) | 37.3 | 23.8 | 23.8 | 10.8 | 24.6 | 24.6 | 68.6 | 65.0 | 65.0 | 56.3 | 56.3 |
| 56.3 |  |  |  |  |  |  |  |  |  |  |  |


| Act Efict Green (s) | 37.3 | 23.8 | 23.8 | 0.8 | 24.6 | 24.6 | 60.6 | 60.0 | 60.0 | 50.3 | 50.3 | 50.49 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 0.32 | 0.21 |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | 0.44 | 0.71 | 0.27 | 0.56 | 0.49 | 0.13 | 0.42 | 0.74 | 0.51 | 0.28 | 0.71 | 0.18 |


|  | 30.4 | 54.1 | 9.9 | 59.0 | 44.7 | 2.1 | 19.5 | 23.1 | 4.0 | 31.9 | 28.0 | 3.9 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Control Delay | 30.6 | 50.1 |  |  |  |  |  |  |  |  |  |  |


| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| otal Delay | 30.6 | 54.1 | 9.9 | 59.0 | 44.7 | 2.1 | 19.5 | 23.1 | 4.0 | 31.9 | 28.0 | 3.9 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| OS | C | D | A | E | D | A | B | C | A | C | C | A |


| Approach Delay | 38.9 | 45.9 | 17.9 | 25.5 |
| :--- | ---: | ---: | ---: | ---: |
| D | D | B | C |  |

## tersection Summary

Area Type:
Cycle Length: 125
Actuated Cycle Len
Natural Cycle: 95
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.74
$\begin{array}{ll}\text { Intersection Signal Delay: } 25.4 & \text { Intersection LOS: C } \\ \text { Intersection Capacity Utilization 91.1\% } & \text { ICU Level of Service F }\end{array}$
Analysis Period (min) 15


200185-12148 Albion Vaughan Road TIS

Queues
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road Future Total: PM Peak Hour

|  | $\Rightarrow$ | $\rightarrow$ | \% | $\checkmark$ | - | 4 | 4 | $\uparrow$ | F | - | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 171 | 256 | 85 | 170 | 172 | 46 | 69 | 1407 | 541 | 27 | 1172 | 141 |
| v/c Ratio | 0.44 | 0.71 | 0.27 | 0.56 | 0.49 | 0.13 | 0.42 | 0.74 | 0.51 | 0.28 | 0.71 | 0.18 |
| Control Delay | 30.6 | 54.1 | 9.9 | 59.0 | 44.7 | 2.1 | 19.5 | 23.1 | 4.0 | 31.9 | 28.0 | 3.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 30.6 | 54.1 | 9.9 | 59.0 | 44.7 | 2.1 | 19.5 | 23.1 | 4.0 | 31.9 | 28.0 | 3.9 |
| Queue Length 50th (m) | 25.3 | 50.1 | 0.0 | 17.7 | 31.7 | 0.0 | 5.9 | 110.5 | 4.4 | 3.4 | 102.0 | 0.0 |
| Queue Length 95th (m) | 40.4 | 75.0 | 11.3 | 30.2 | 50.8 | 1.8 | 14.1 | 161.5 | 23.9 | 12.6 | 145.0 | 10.7 |
| Internal Link Dist (m) |  | 265.2 |  |  | 528.1 |  |  | 354.1 |  |  | 662.1 |  |
| Turn Bay Length (m) | 100.0 |  | 90.0 | 170.0 |  | 70.0 | 125.0 |  | 180.0 | 35.0 |  | 150.0 |
| Base Capacity (vph) | 389 | 500 | 399 | 311 | 485 | 442 | 166 | 1897 | 1054 | 95 | 1660 | 805 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.44 | 0.51 | 0.21 | 0.55 | 0.35 | 0.10 | 0.42 | 0.74 | 0.51 | 0.28 | 0.71 | 0.18 |

HCM Signalized Intersection Capacity Analysis
1: Regional Road 50 \& Mayfield Road/Albion Vaughan Road
Future Total: PM Peak Hour

|  | $\rangle$ | $\rightarrow$ |  | $\downarrow$ |  |  | 4 | $\uparrow$ | P |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | $\uparrow$ | ${ }^{7}$ | 9* | $\uparrow$ | F' | \% | ¢ $\uparrow$ | " | \% | 个个 |  |
| Trafic Volume (vph) | 171 | 256 | 85 | 170 | 172 | 46 | 69 | 1407 | 541 | 27 | 1172 | 141 |
| Future Volume (vph) | 171 | 256 | 85 | 170 | 172 | 46 | 69 | 1407 | 541 | 27 | 1172 | 141 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 |
| Total Lost time (s) | 3.0 | 6.5 | 6.5 | 3.0 | 6.5 | 6.5 | 3.0 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1684 | 1746 | 1183 | 3267 | 1642 | 1298 | 1182 | 3380 | 1493 | 1513 | 3411 | 1507 |
| Flt Permitted | 0.58 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.13 | 1.00 | 1.00 | 0.12 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1034 | 1746 | 1183 | 3267 | 1642 | 1298 | 160 | 3380 | 1493 | 198 | 3411 | 1507 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 171 | 256 | 85 | 170 | 172 | 46 | 69 | 1407 | 541 | 27 | 1172 | 141 |
| RTOR Reduction (vph) | 0 | , | 68 | , | 0 | 36 | 0 | 0 | 214 |  | 0 |  |
| Lane Group Flow (vph) | 171 | 256 | 17 | 170 | 172 | 10 | 69 | 1407 | 327 | 27 | 1172 | 68 |
| Heavy Vehicles (\%) | 6\% | 10\% | 35\% | 6\% | 17\% | 23\% | 51\% | 8\% | 7\% | 18\% | 7\% | 6\% |
| Turn Type | pm+pt | NA | Perm | Prot | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 1 | - |  |  | 2 |  |
| Permitted Phases | 4 |  | 4 |  |  |  | 6 |  | 6 | 2 |  |  |
| Actuated Green, G (s) | 33.8 | 23.8 | 23.8 | 10.8 | 24.6 | 24.6 | 65.6 | 65.6 | 65.6 | 56.3 | 56.3 | 56. |
| Effective Green, $\mathrm{g}(\mathrm{s})$ | 33.8 | 23.8 | 23.8 | 10.8 | 24.6 | 24.6 | 65.6 | 65.6 | 65.6 | 56.3 | 56.3 | 56.3 |
| Actuated g/C Ratio | 0.29 | 0.20 | 0.20 | 0.09 | 0.21 | 0.21 | 0.56 | 0.56 | 0.56 | 0.48 | 0.48 | 0.48 |
| Clearance Time (s) | 3.0 | 6.5 | 6.5 | 3.0 | 6.5 | 6.5 | 3.0 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |
| Vehicle Extension (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | 356 | 357 | 242 | 303 | 347 | 274 | 145 | 1906 | 842 | 95 | 1651 | 729 |
| v/s Ratio Prot | 0.04 | c0.15 |  | c0.05 | 0.10 |  | 0.03 | c0.42 |  |  | 0.34 |  |
| v/s Ratio Perm | 0.10 |  | 0.01 |  |  | 0.01 | 0.24 |  | 0.22 | 0.14 |  | 0.05 |
| v/c Ratio | 0.48 | 0.72 | 0.07 | 0.56 | 0.50 | 0.04 | 0.48 | 0.74 | 0.39 | 0.28 | 0.71 | 0.09 |
| Uniform Delay, d1 | 32.6 | 43.1 | 37.3 | 50.5 | 40.4 | 36.4 | 16.0 | 18.9 | 14.1 | 17.9 | 23.6 | 16. |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.0 |
| Incremental Delay, d2 | 2.1 | 8.3 | 0.3 | 3.9 | 2.3 | 0.1 | 5.1 | 2.6 | 1.3 | 7.4 | 2.6 | 0.3 |
| Delay (s) | 34.7 | 51.4 | 37.6 | 54.4 | 42.7 | 36.5 | 21.1 | 21.5 | 15.5 | 25.3 | 26.2 | 16. |
| Level of Service | C | D | D | D | D | D | C | C | B | C | C |  |
| Approach Delay (s) |  | 43.5 |  |  | 47.1 |  |  | 19.9 |  |  | 25.2 |  |
| Approach LOS |  | D |  |  | D |  |  | B |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 26.9 |  | HCM 2000 | Level of S | Service |  | C |  |  |  |
| HCM 2000 Control Delay <br> HCM 2000 Volume to Capacity ratio |  |  | 0.73 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 116.3 |  | Sum of los | time (s) |  |  | 19.1 |  |  |  |
| Intersection Capacity Utilization |  |  | 91.1\% |  | CU Level | ff Service |  |  | F |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

## 200185-12148 Albion Vaughan Road TIS

Synchro 10 Report

## Appendix I

## AutoTURN Analysis - Vehicle Maneuvering Diagrams

Fire route assessment. Fire truck, inbound and outbound movements


Waste Truck Loading area assessment. Inbound and outbound movements. North Tower


Waste Truck Loading area assessment. Inbound and outbound movements. South Tower


Typical Delivery Vehicle Loading area assessment. Inbound and outbound movements. North Tower


Typical Delivery Vehicle Loading area assessment. Inbound and outbound movements. South Tower


Passenger Vehicle circulation at-grade.
Inbound and outbound movements.


Passenger Vehicle circulation within underground level 1.


Passenger Vehicle circulation within underground level 2.



[^0]:    1 Regional Municipality of Peel, Traffic Impact Study Guidelines, Accessed 9 November 2020 from https://www.peelregion.ca/pw/transportation/business/traffic-impact-study.asp

[^1]:    2 Town of Caledon, Official Plan, Schedule J - Long Range Road Network, April 2018.

    3 Regional Municipality of Peel, Official Plan, Schedule F-2 - Major Road Network, April 2022.

[^2]:    4 Regional Municipality of Peel, Active Transportation Implementation Plan 20182022.

[^3]:    5 https://data.peelregion.ca/datasets/844846e93de64ddd910c2b6e964105f1_ 0/explore?location=43.846124\%2C-79.693155\%2C16.21

[^4]:    6 Regional Municipality of Peel, Traffic Impact Study Guidelines, Accessed 9 November 2020 from https://www.peelregion.ca/pw/transportation/business/traffic-impact-study.asp

[^5]:    7 Regional Municipality of Peel, Regional Guidelines for Using Synchro Version 7.73 Rev 8, December 2010.

    8 Regional Municipality of Peel, Regional Guidelines for Using Synchro Version 7.73 Rev 8, December 2010.

[^6]:    9 Institute of Transportation Engineers, Trip Generation Manual (11th Edition), September 2021.

[^7]:    10 Town of Caledon, Zoning By-law, Section 5: Parking, Loading and Delivery Standards, February 102022.

[^8]:    11 Town of Caledon, Zoning By-law 2015-58, Schedule K: Designed Accessible Parking Spaces, Effective 27 April 2021.

[^9]:    200185-12148 Albion Vaughan Road TIS
    Synchro 10 Report

[^10]:    200185-12148 Albion Vaughan Road TIS
    PTSL

[^11]:    200185-12148 Albion Vaughan Road TIS
    Synchro 10 Report

[^12]:    200185-12148 Albion Vaughan Road TIS
    PTSL

[^13]:    200185-12148 Albion Vaughan Road TIS
    Synchro 10 Report

[^14]:    200185-12148 Albion Vaughan Road TIS
    PTSL

[^15]:    200185-12148 Albion Vaughan Road TIS
    Synchro 10 Report

[^16]:    200185-12148 Albion Vaughan Road TIS
    PTSL

[^17]:    200185-12148 Albion Vaughan Road TIS
    Synchro 10 Report

[^18]:    200185-12148 Albion Vaughan Road TIS
    PTSL

[^19]:    200185-12148 Albion Vaughan Road TIS
    Synchro 10 Report

[^20]:    200185-12148 Albion Vaughan Road TIS
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[^22]:    200185-12148 Albion Vaughan Road TIS

[^23]:    200185-12148 Albion Vaughan Road TIS

[^24]:    200185-12148 Albion Vaughan Road TIS

